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A SUMMARY OF THE NUMERICAL RESULTS OF A THEORETICAL STUDY OF THE SCATTERING OF NEUTRONS BY COMPLEX NUCLEI

Ву

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## SUMMARY OF THE NUMERICAL RESULTS OF A THEORETICAL STUDY OF THE SCATTERING OF NEUTRONS BY COMPLEX NUCLEI

#### I. INTRODUCTION

#### A. General Remarks

The purpose of this report is to achieve the presentation in convenient reference form of the numerical results of a theoretical study of the scattering of neutrons by complex nuclei. Only quantities which are plotted or tabulated in this report will be discussed here. Publication in the Physical Review of a paper covering in more detail the physically important results of this study is being planned for the near future. The numerical computations for this report were carried out by Elgie Ginsburgh, Barbara Levine, and Hannah Wasserman of the Joint Computing Group. Grace Rowe performed the necessary drafting work.

#### B. Total Cross Section

Under the assumption that there is no potential acting on a neutron which is outside of a target nucleus, both the total cross section and the differential cross section for elastic scattering can be expressed in a form such that the entire dependence of these cross sections on target properties is contained in the logarithmic derivative of the neutron wave function evaluated at the surface of the target nucleus. Considering the neutron to have an effective spin of zero, one can write the total cross section as

<sup>◆</sup> J. M. Blatt and V. F. Weisskopf, <u>Theoretical Nuclear Physics</u>
(John Wiley and Sons, Inc., New York, 1952) Chapter VIII.

$$\frac{\sigma_{t}}{\pi R^{2}} = \sum_{\ell=0}^{\infty} \frac{\sigma_{t}^{(\ell)}}{\pi R^{2}}$$

$$\frac{\sigma_{t}^{(\ell)}}{\pi R^{2}} = \frac{2!+1}{\pi^{2}} 2(\text{Re}(1-\gamma_{\ell})), \qquad (1)$$

where x=kR. R is the nuclear radius, and k is the wave number of the incident neutron.  $\eta_{\varrho}$  is given by the equation

with

$$M_{R} = -Imf_{R} + s_{R} ,$$

$$N_{R} = Ref_{R} - \Delta_{R} .$$
(3)

is the logarithmic derivative of the product of the neutron radial coordinate and the radial wave function evaluated at the surface of the target nucleus.  $\Delta_{\mathcal{Q}}$ ,  $s_{\mathcal{Q}}$ , and  $\delta_{\mathcal{Q}}$  depend upon x only and are given by the expressions

$$\Delta_{\underline{q}} + is_{\underline{q}} = 1 + \frac{xh_{\underline{q}}^{\dagger}(x)}{h_{\underline{q}}(x)},$$

$$\delta_{\underline{q}} = \tan^{-1}\left(-\frac{j_{\underline{q}}(x)}{n_{\underline{q}}(x)}\right).$$
(4)

Here  $h_{\ell}$  is a spherical Hankel function, and  $j_{\ell}$  and  $n_{\ell}$  are spherical Bessel functions.

Combining Eq. (2) with Eqs. (1) yields

$$\frac{\sigma_{t}^{(\ell)}}{\pi^{R^{2}}} = \frac{1}{\pi^{2}} (2\ell+1) \left[ \sin^{2} \delta_{\ell} + s_{\ell} \frac{M_{\ell} \cos^{2} \delta_{\ell} - N_{\ell} \sin^{2} \delta_{\ell}}{M_{\ell}^{2} + N_{\ell}^{2}} \right],$$

$$\frac{\sigma_{t}}{\pi^{R^{2}}} = \sum_{\ell=0}^{\infty} \frac{\sigma_{t}^{(\ell)}}{\pi^{R^{2}}}.$$
(5)

Once f has been specified via some nuclear model, Eqs. (3) and (5) together with the tables of Section VI of this report constitute a complete base for the numerical computation of the neutron total cross section.

In Sections II and III plots of  $\sigma_t/\pi R^2$  are given for a nuclear model specified by the potential function (r is the neutron radial coordinate)

$$V(\mathbf{r}) = \begin{cases} -V_0(1+i\zeta), & \mathbf{r} < R \\ 0, & \mathbf{r} > R \end{cases}$$
 (6)

This gives an  $f_{R}$  of the form

$$f_{Q} = 1 + \frac{Xj_{Q}^{*}(X)}{j_{Q}(X)},$$
 (7)

where

$$x^{2} = x^{2} + X_{o}^{2} (1+i\zeta),$$

$$x_{o}^{2} = \frac{2m}{\pi^{2}} V_{o} R^{2},$$

$$x^{2} = \frac{2m}{\pi^{2}} ER^{2},$$
(8)

and m is the mass of the neutron.

<sup>\*</sup> Strictly speaking, the reduced mass of the neutron should be used here and all calculations referred to the center-of-mass system. This correction is not important for heavier nuclei.

If we let

$$f_{\ell} = w_{1\ell} - iw_{2\ell},$$

$$X = X_1 + iX_2,$$
(9)

it is found that the recurrence relations for the w's are

$$w_{1R} = \frac{(x_1^2 - x_2^2)(1 - w_{1,R-1}) + 2x_1 x_2 w_{2,R-1}}{(1 - w_{1,R-1})^2 + w_{2,R-1}^2} - R,$$

$$w_{2\hat{k}} = \frac{(x_1^2 - x_2^2)w_{2,k-1}^2 - 2x_1x_2(k-w_{1,k-1})}{(k-w_{1,k-1})^2 + w_{2,k-1}^2},$$

where

$$x_1^2 - x_2^2 = x^2 + x_0^2$$
,  
 $2x_1x_2 = \zeta x_0^2$ . (10)

To start the recurrence relations we have

$$w_{1,0} = \text{Re}(X \cot X) = \frac{X_1 \cot X_1 \csc^2 X_2 + X_2 \coth X_2 \csc^2 X_2}{\cot^2 X_1 + \coth^2 X_2}$$
, (11)

$$w_{2,0} = -Im(XcotX) = \frac{X_1cothX_2csc^2X_1-X_2cotX_1csch^2X_2}{cot^2X_1+coth^2X_2}$$
,

with  $X_1$  and  $X_2$  given by the equations

$$X_{1} = (\frac{1}{2} (x^{2} + X_{0}^{2}) + \frac{1}{2} ((x^{2} + X_{0}^{2})^{2} + (\zeta X_{0}^{2})^{2})^{1/2})^{1/2},$$

$$X_{2} = (-\frac{1}{2} (x^{2} + X_{0}^{2}) + ((x^{2} + X_{0}^{2})^{2} + (\zeta X_{0}^{2})^{2})^{1/2})^{1/2}.$$
(12)

In all the plots of Sections II and III the value of  $\zeta$  is  $\zeta = 0.05$ . This value seemed to give a reasonably good representation of the experimental data on total cross sections reported by Barschall\*. The values of x range from 0.1 to 3.0,  $\overline{\phantom{a}}$  H. H. Barschall, Phys. Rev. 86, 431 (1952).

and those of  $X_0^2$  range from 2.5 to 80. In general, the computed values of the total cross section are accurate to better than five per cent, and in most cases the uncertainty is less than three per cent.

#### C <u>Differential Cross Section for Elastic Scattering</u>

The relevant formula for the differential cross section for elastic scattering is\*

$$\frac{1}{\pi R^2} \frac{d\sigma_{el}}{d\Omega} = \frac{1}{x^2} \left| \sum_{\ell=0}^{\infty} (2\ell+1)^{1/2} (1-\gamma_{\ell}) Y_{\ell,0}(\theta) \right|^2, \tag{13}$$

which can be written

$$\frac{1}{\pi R^2} \frac{d\sigma_{el}}{d\Omega} = \frac{1}{x^2} \left[ (\text{Re} \Sigma)^2 + (\text{Im} \Sigma)^2 \right], \qquad (14)$$

where, since  $Y_{\ell,0} = (2\ell + 1/4\pi)^{1/2} P_{\ell}(\cos\theta)$ ,

Re 
$$\sum = (4\pi)^{-1/2} 2 \sum_{\ell=0}^{\infty} (2\ell+1) \left[ \sin^2 \delta_{\ell} + s_{\ell} \frac{M_{\ell} \cos 2\delta_{\ell} - N_{\ell} \sin 2\delta_{\ell}}{M_{\ell}^2 + N_{\ell}^2} \right] P_{\ell} (\cos \theta),$$

$$= (4\pi)^{-1/2} \frac{x^2}{2} \sum_{k=0}^{\infty} \frac{\sigma_k^{(k)}}{\pi R^2} P_k(\cos\theta), \qquad (15)$$

Im 
$$\sum = (4\pi)^{-1/2} \sum_{\ell=0}^{\infty} (2\ell+1) \left[ \sin 2\delta_{\ell} - 2s_{\ell} \frac{M_{\ell} \sin 2\delta_{\ell} + N_{\ell} \cos 2\delta_{\ell}}{M_{\ell}^2 + N_{\ell}^2} \right] P_{\ell} (\cos \theta)$$
.

When  $f_{R}$  is given, Eqs. (3), (14), and (15) and the tables of Section VI are sufficient for the computation of the differential cross section for elastic scattering.

<sup>\*</sup> Blatt and Weisskopf, loc. cit.

In Section IV differential cross sections for elastic scattering are plotted using the  $f_{\ell}$  of Eq. (7). The ratio of  $x^2$  to  $X_0^2$  is fixed at 1/19 corresponding to 1 MeV incident neutrons with a 19 MeV well depth.  $\zeta$  is set equal to 0.05, and  $X_0^2$  ranges from 4.75 to 83.79. The uncertainty in computed values is less than five per cent.

The differential cross sections of Section VI do not include the possibility of elastic scattering via compound nucleus formation. By providing a mechanism for compound nucleus formation with elastic reemission analogous to that of Feshbach, Peaslee, and Weisskopf and including also the possibility of independent particle scattering, it is found that on averaging over the narrow fine-structure resonances the resulting differential cross section for elastic scattering is the same as that of Eq. (14) with the exception of a term of the form

$$\sum_{\theta=0}^{\infty} \frac{\sigma_{c\theta}^{(\ell)}}{\pi R^2} \left| Y_{\ell,0}(\theta) \right|^2 , \qquad (16)$$

which must be added on the right-hand side of Eq. (14) where

$$\frac{\sigma_{ce}^{(\ell)}}{\pi R^2} = \frac{1}{x^2} (2\ell + 1) s_{\ell} \frac{(-Imf_{\ell})}{M_{\ell}^2 + N_{\ell}^2}, \qquad (17)$$

is the partial cross section for compound-elastic scattering.

Eq. (17) has the <u>form</u> of a reaction cross section with for given by Eq. (9) since no actual absorption is present. The quantity used in the plots of Section V is <u>not</u> an absorption

<sup>+</sup> H. Feshbach, D. C. Peaslee, and V. F. Weisskopf, Phys. Rev. 71, 145 (1947).

<sup>/</sup> This has been called capture-elastic scattering by some authors.

parameter; it specifies the strength of the coupling between the incident neutron and target nucleus which leads to elastic scattering via the intermediary of compound nucleus formation. No net loss of particles is involved. It is evident from the  $|Y_{R}, 0|^2$  in Eq. (16) that this additional term is symmetric about an angle of  $90^{\circ}$ .

The two sets of differential cross sections for elastic scattering represent extremes. One set corresponds to absorption and no compound-elastic scattering, while the other corresponds to compound-elastic scattering and no absorption. Both sets, of course, contain the independent-particle features.

Section V contains the plots of the averaged differential cross section. The values of  $\xi$ ,  $x^2$ , and  $X_0^2$  are the same as those used in Section IV. The uncertainty in the computed values is less than five per cent.

#### D. Tables

Section VI of this report contains tables of quantities important for neutron-cross-section calculations that depend upon x only (see Eq. (4)), i.e. that do not depend upon a specific model for the internal structure of the target nucleus.

One can obtain  $\cos 2\delta_{\underline{a}}$ ,  $\sin 2\delta_{\underline{a}}$ , and  $\sin^2 \delta_{\underline{a}}$  either by using tables of  $\delta_{\underline{a}}$  or by using tables of  $j_{\underline{a}}$  (x) and  $n_{\underline{a}}$  (x) and the formulas

<sup>◆</sup> A. N. Lowan, P. M. Morse, H. Feshbach, and M. Lax, <u>Scattering</u> and <u>Radiation from Circular Cylinders and Spheres</u>, February, 1945.

$$\cos 2 \frac{x}{2} = \frac{1 - j_{\ell}^{2}(x) / n_{\ell}^{2}(x)}{1 + j_{\ell}^{2}(x) / n_{\ell}^{2}(x)} ,$$

$$\sin 2\delta_{\mathbf{g}} = -\frac{2j_{\mathbf{g}}(\mathbf{x})/n_{\mathbf{g}}(\mathbf{x})}{1+j_{\mathbf{g}}^{2}(\mathbf{x})/n_{\mathbf{g}}^{2}(\mathbf{x})},$$
 (18)

$$\sin^2 \delta_{\mathbf{g}} = \frac{j_{\mathbf{g}}^2(\mathbf{x})/n_{\mathbf{g}}^2(\mathbf{x})}{1+j_{\mathbf{g}}^2(\mathbf{x})/n_{\mathbf{g}}^2(\mathbf{x})}.$$

From Eq. (4) and the recurrence relations for the spherical Hankel functions, it is possible to show that

$$\Delta_{\mathbf{g}} = \frac{\mathbf{x}^{2}(\mathbf{g} - \Delta_{\mathbf{g}-1})}{(\mathbf{g} - \Delta_{\mathbf{g}-1})^{2} + \mathbf{s}_{\mathbf{g}-1}^{2}} - \mathbf{g} ,$$

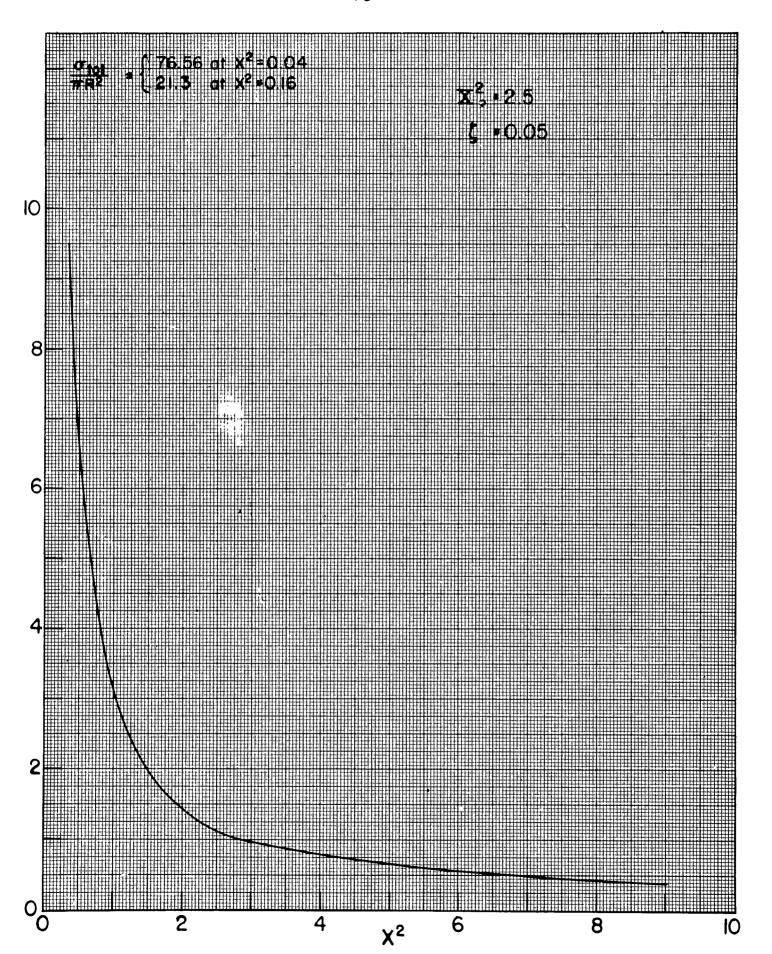
$$\mathbf{s}_{\mathbf{g}} = \frac{\mathbf{x}^{2}\mathbf{s}_{\mathbf{g}-1}}{(\mathbf{g} - \Delta_{\mathbf{g}-1})^{2} + \mathbf{s}_{\mathbf{g}-1}^{2}} .$$
(19)

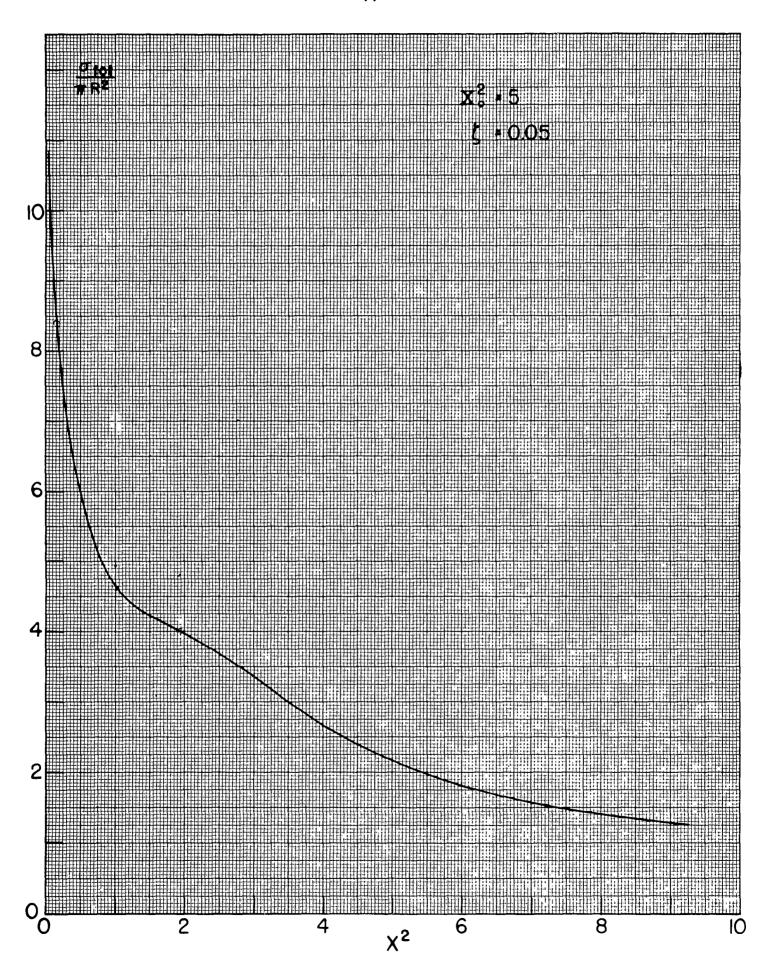
To start these recurrence relations, we have

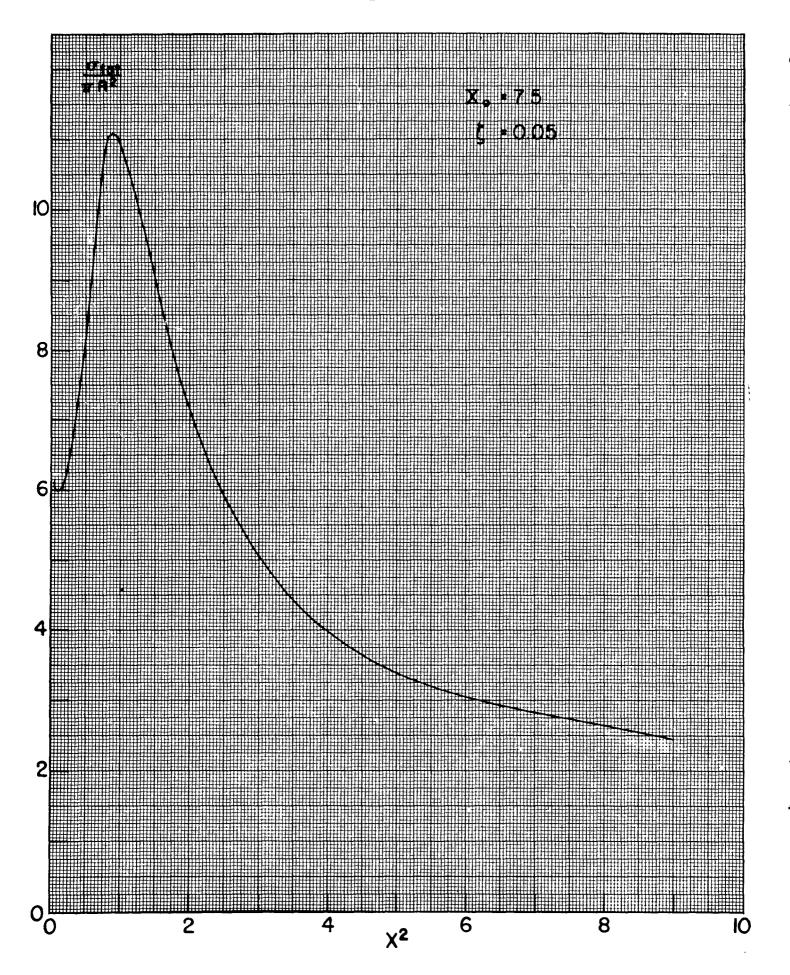
$$\Delta_{0} = 0 , \qquad (20)$$

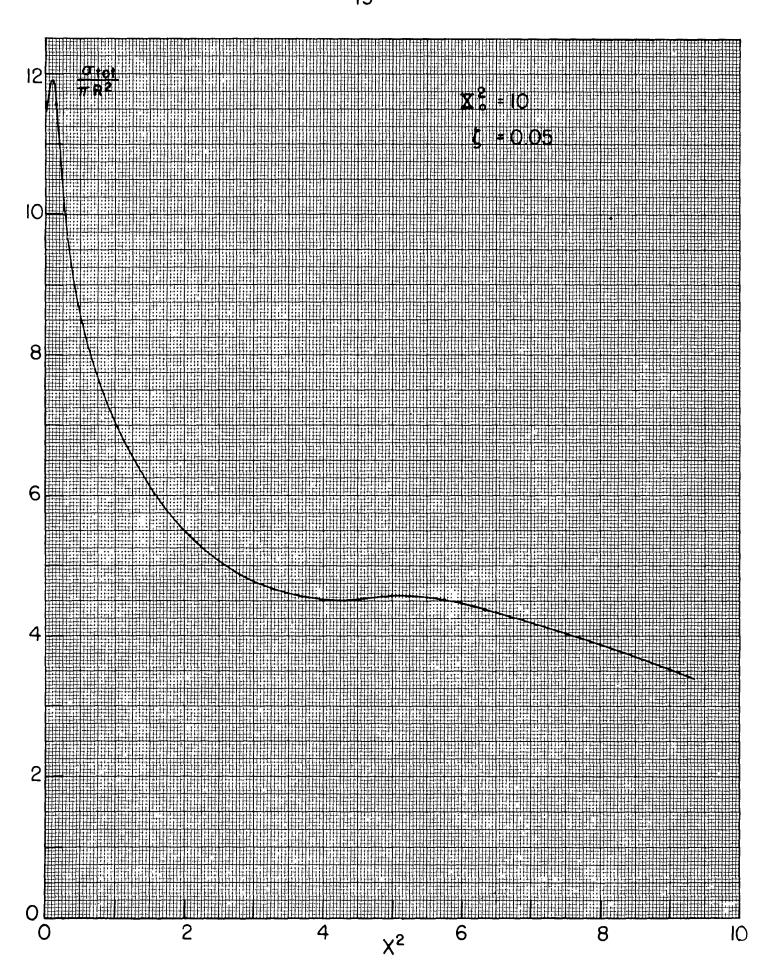
In Section VI, tables of  $s_{\ell}$ ,  $\Delta_{\ell}$ ,  $\cos 2\delta_{\ell}$ ,  $\sin 2\delta_{\ell}$ , and  $\sin^2 \delta_{\ell}$  are given for values of x from 0.1 to 3.0 in steps of 0.1 and for values of  $\ell$  from 0 to 7 inclusive. The tables are accurate to  $\pm$  1 in the last digit.

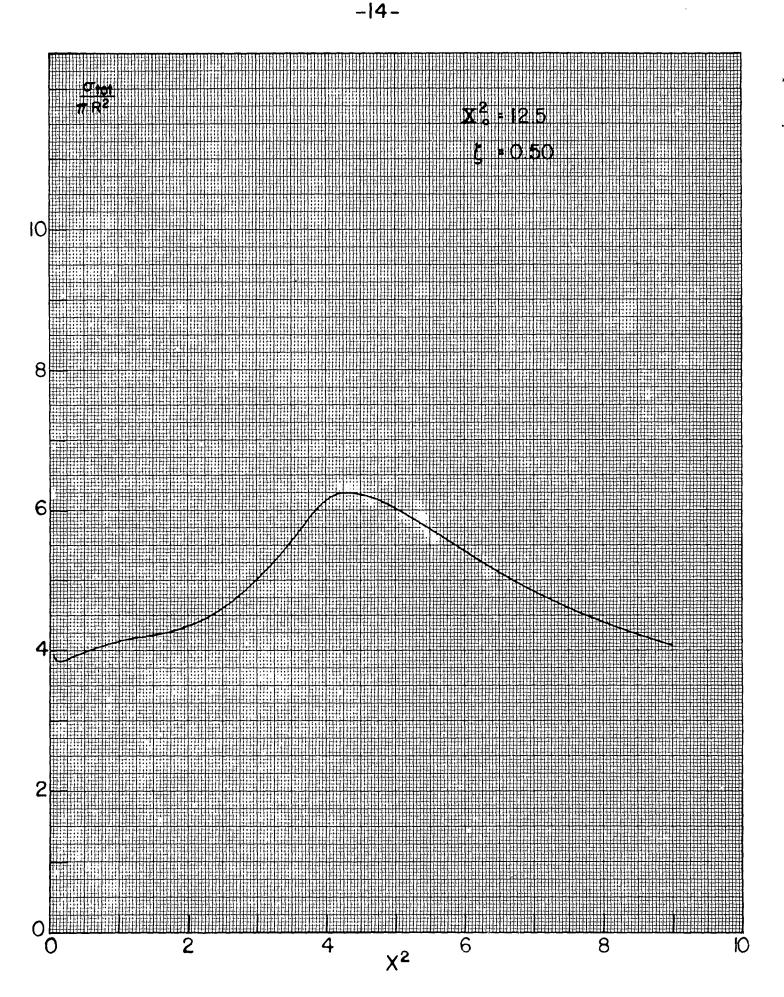
II. PLOTS OF TOTAL CROSS SECTION VS.  $x^2$  FOR FIXED  $x_0^2$  WITH  $\xi = 0.05$ 

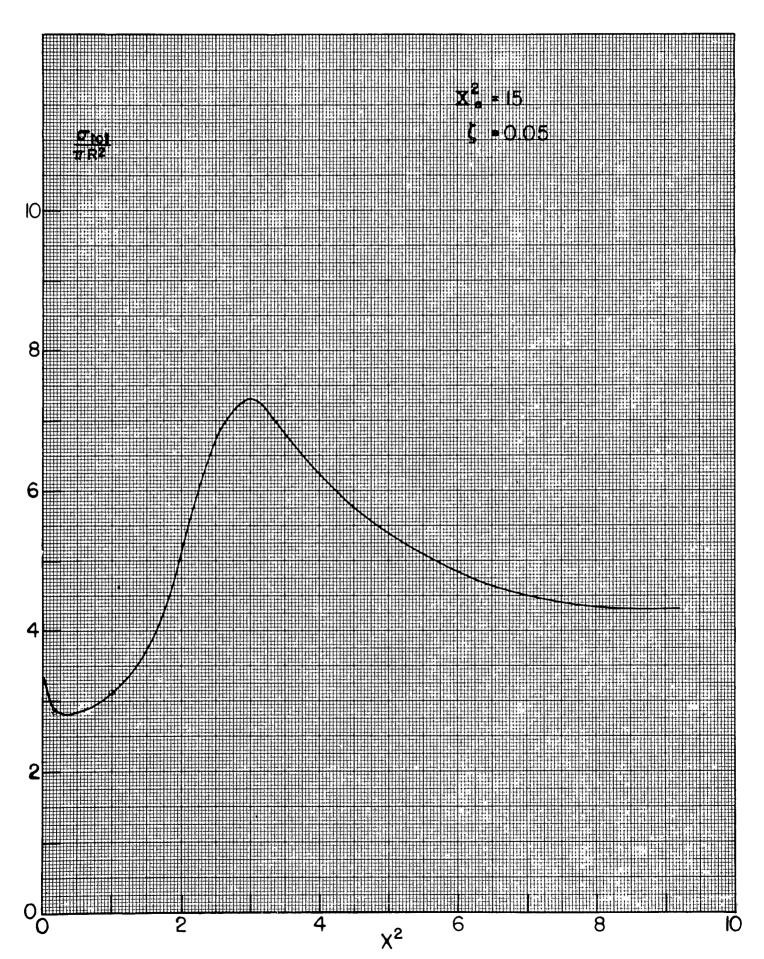


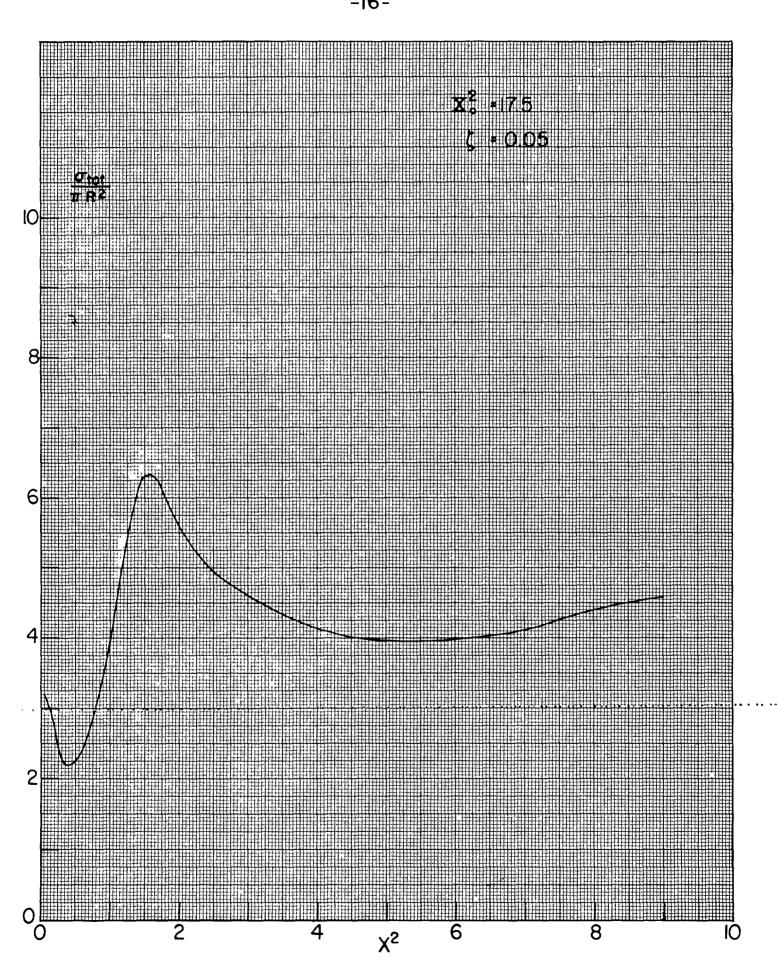


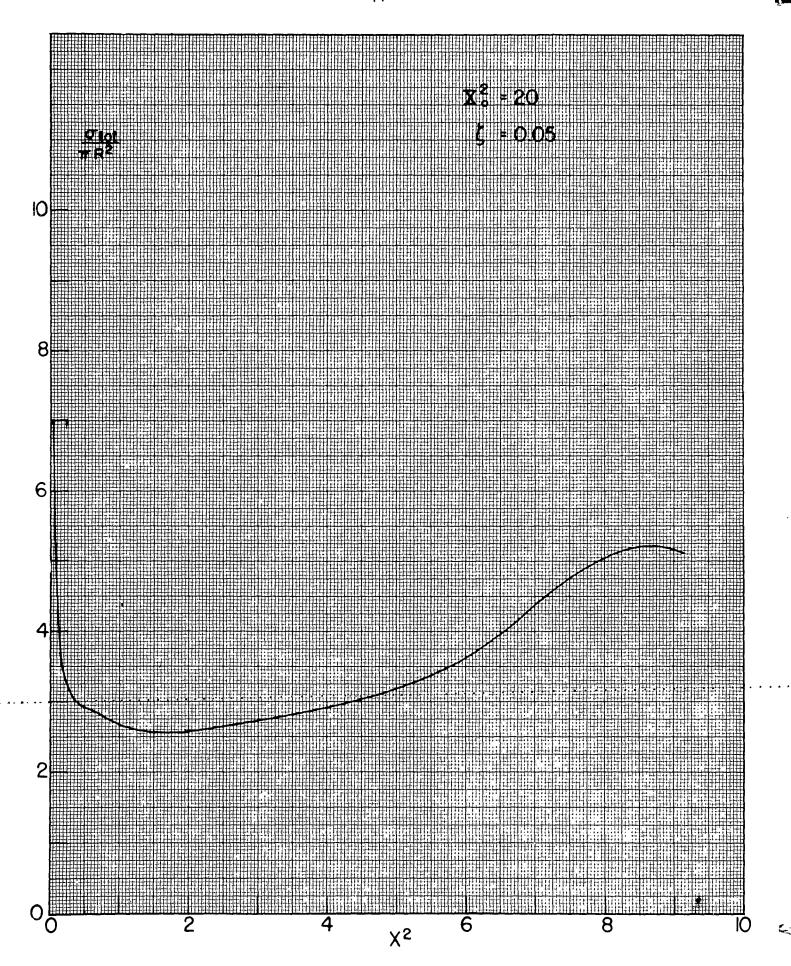


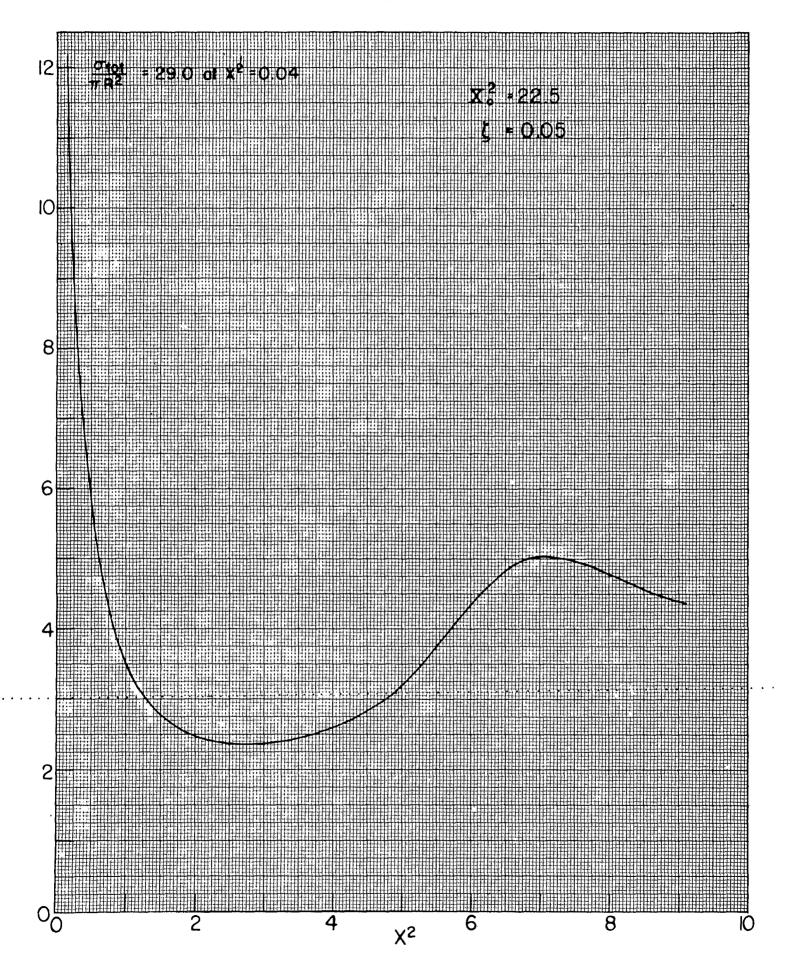


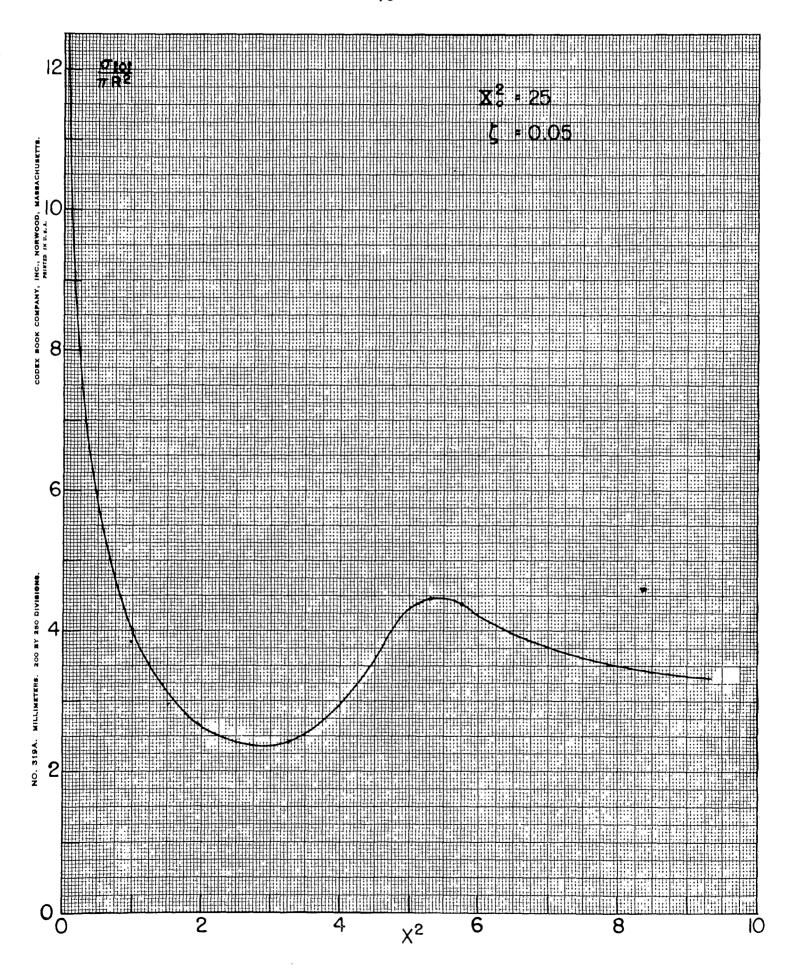




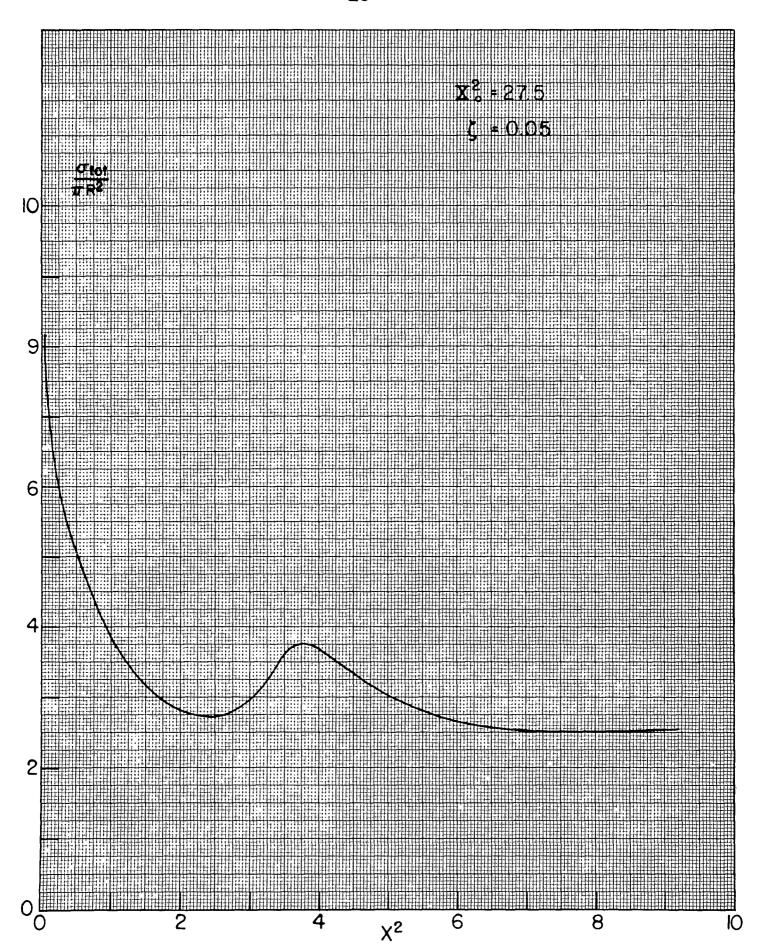


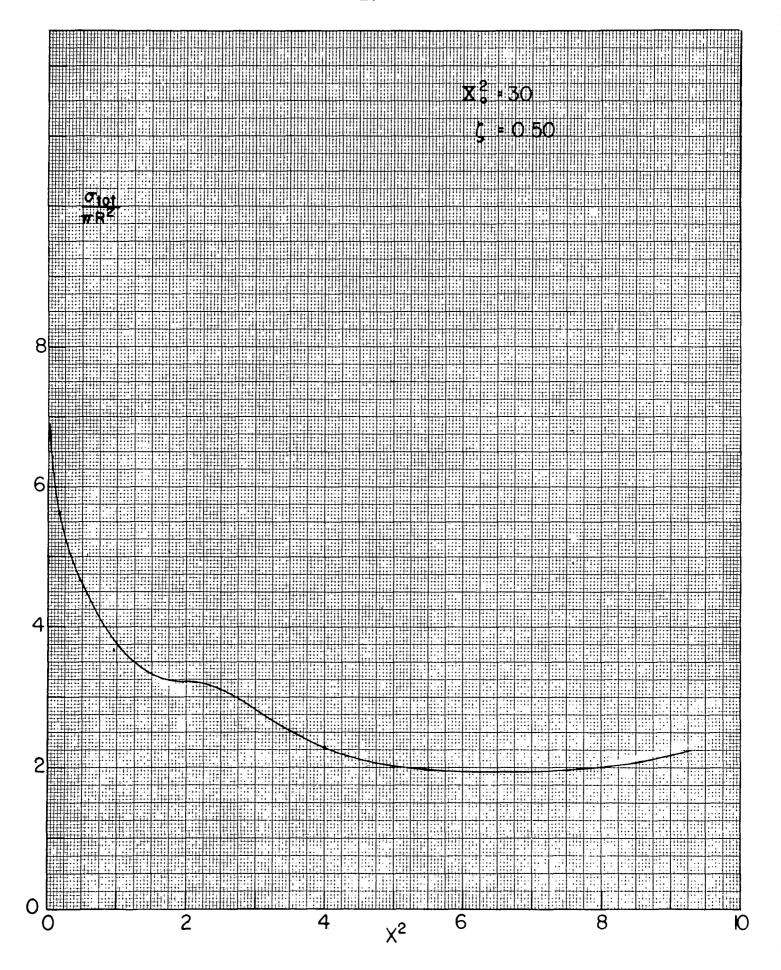


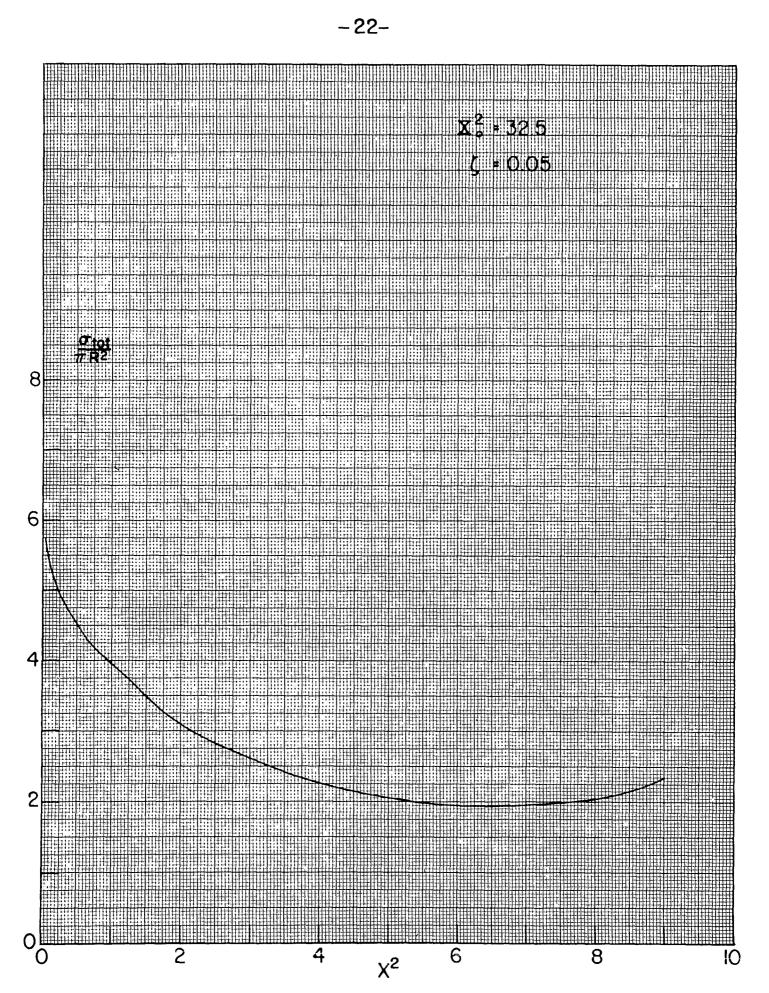




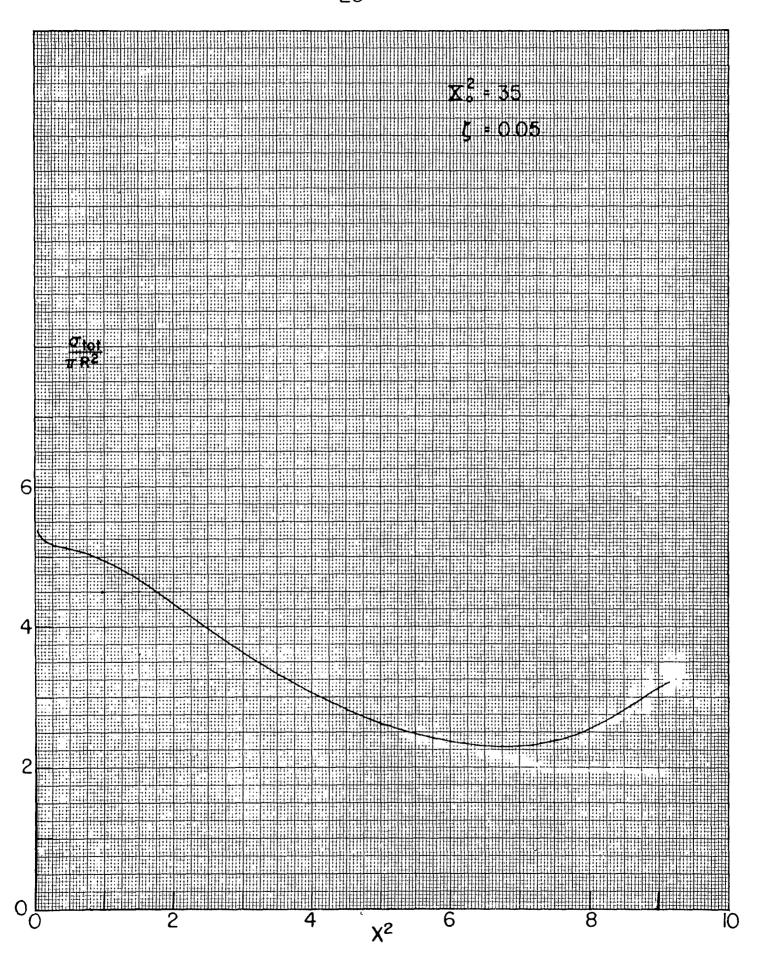
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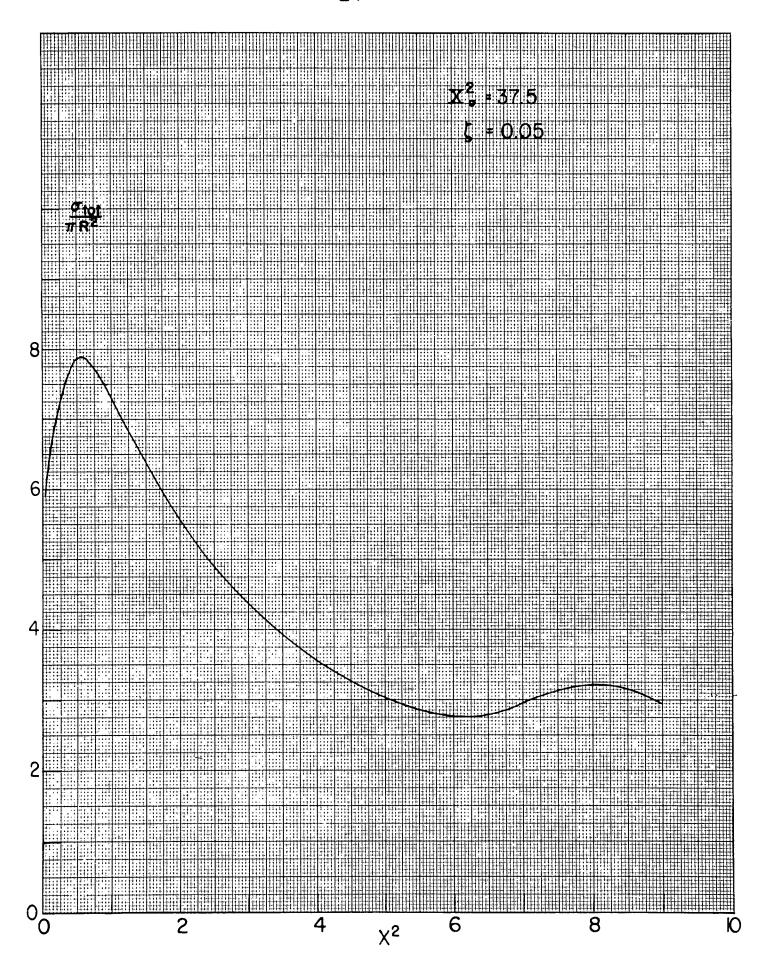


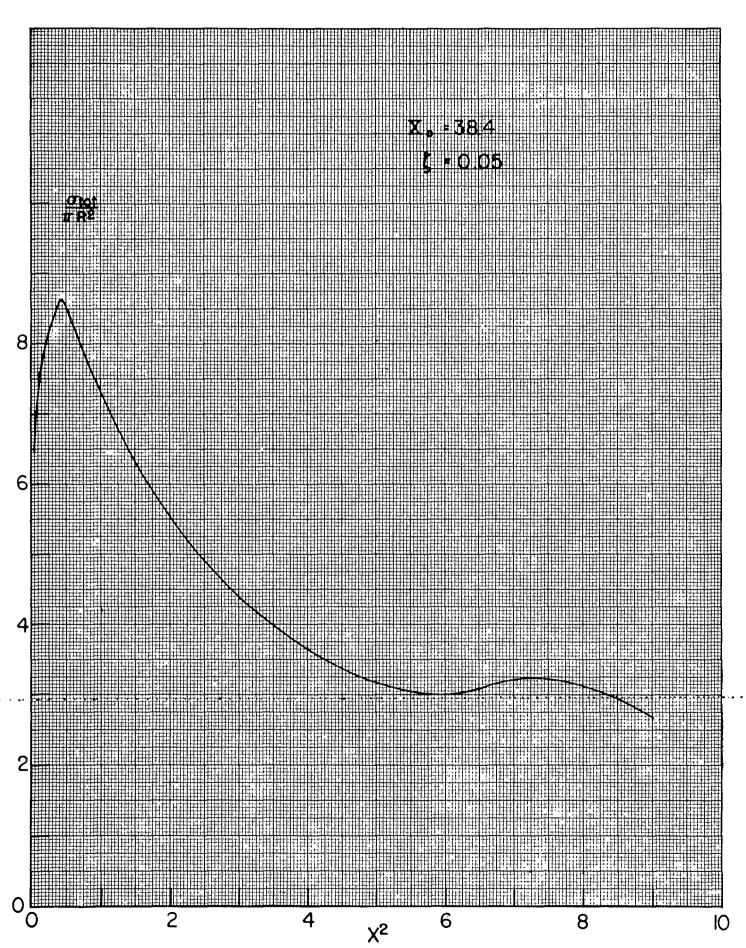


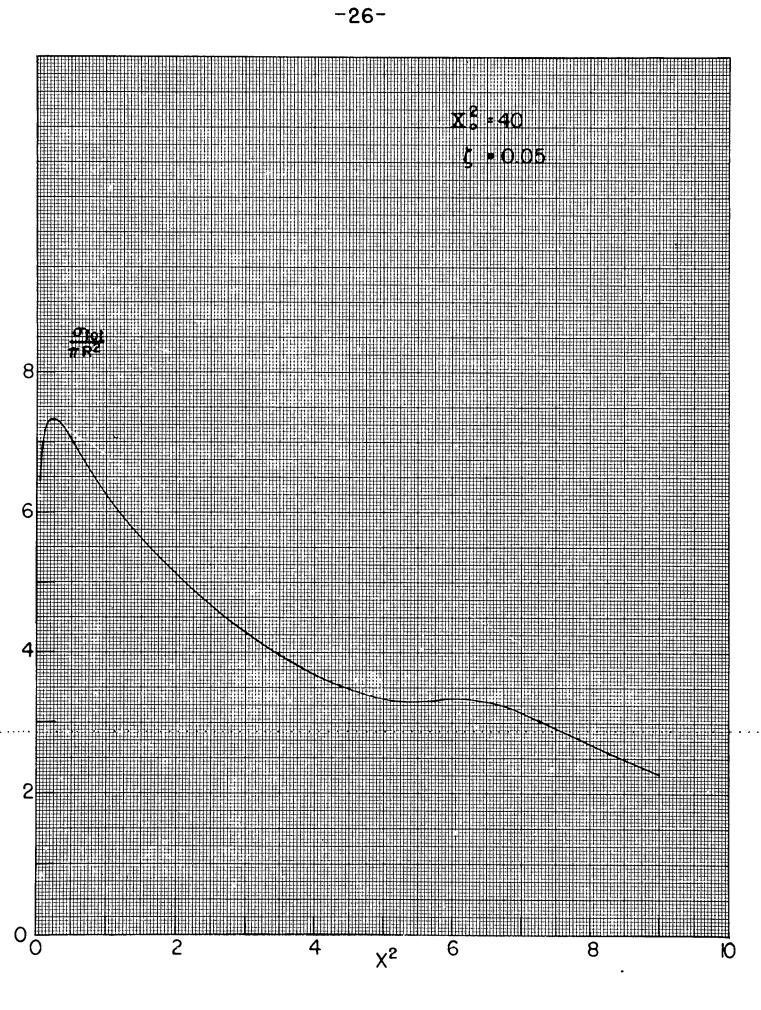


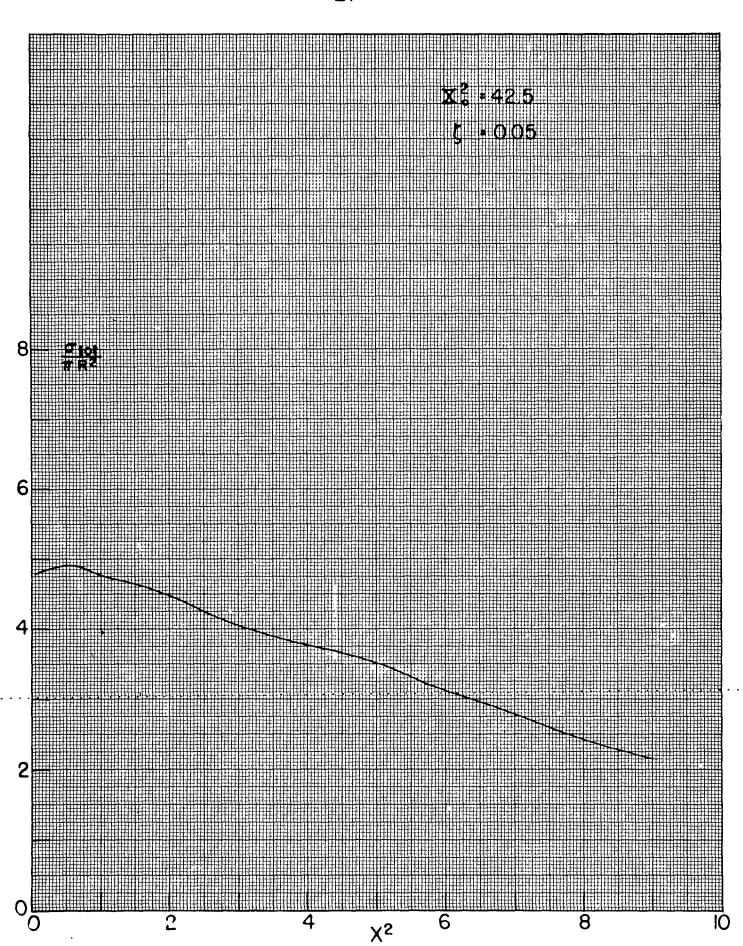
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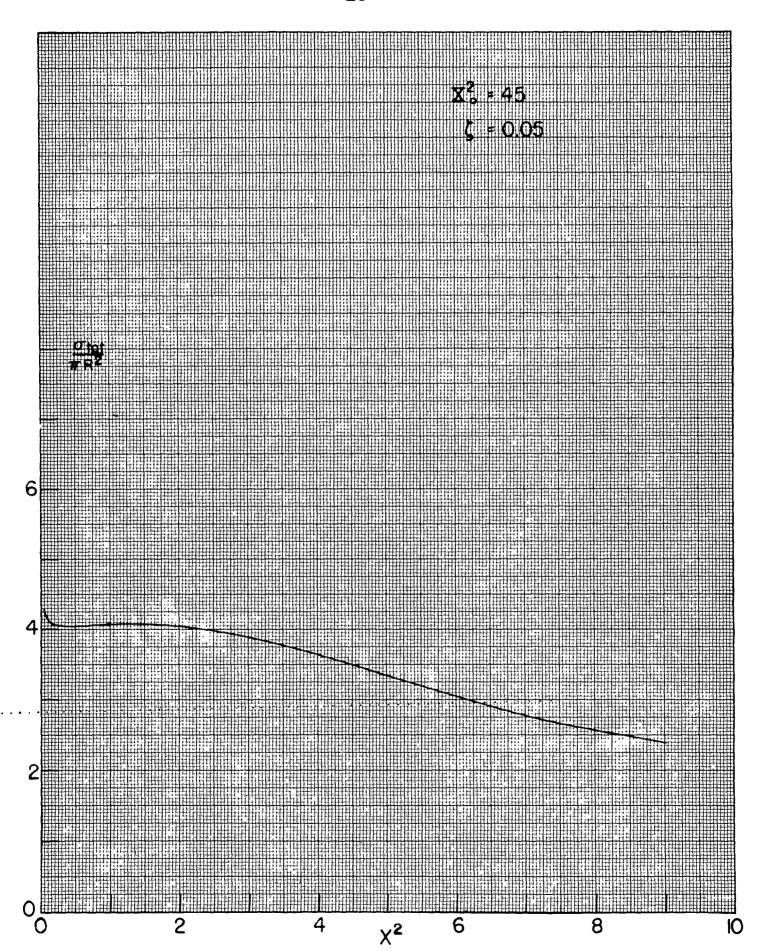


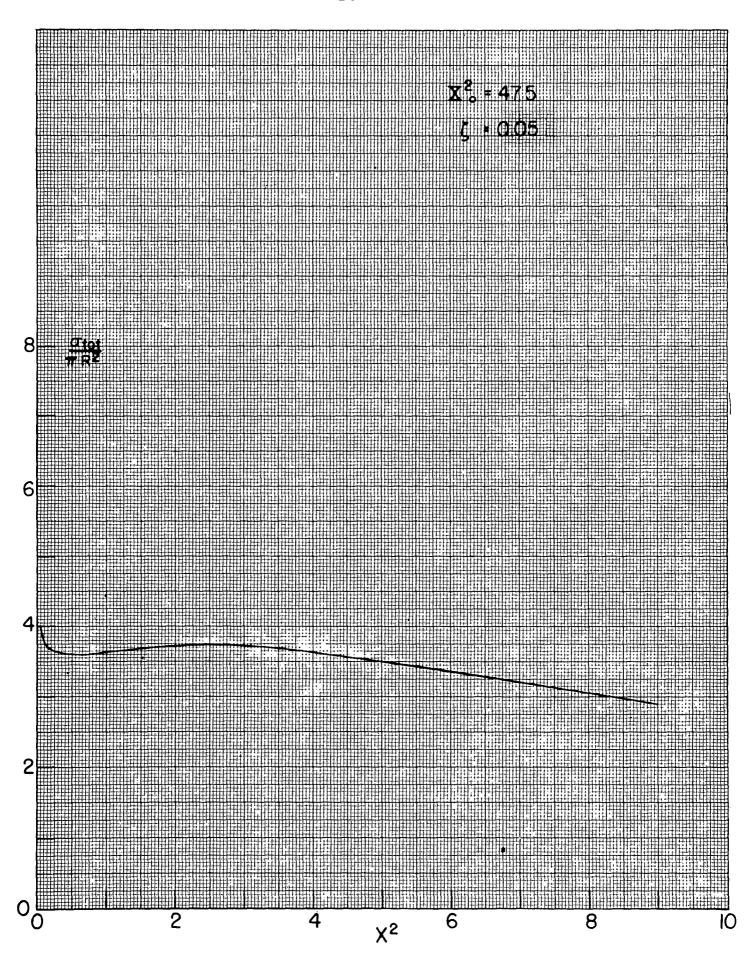


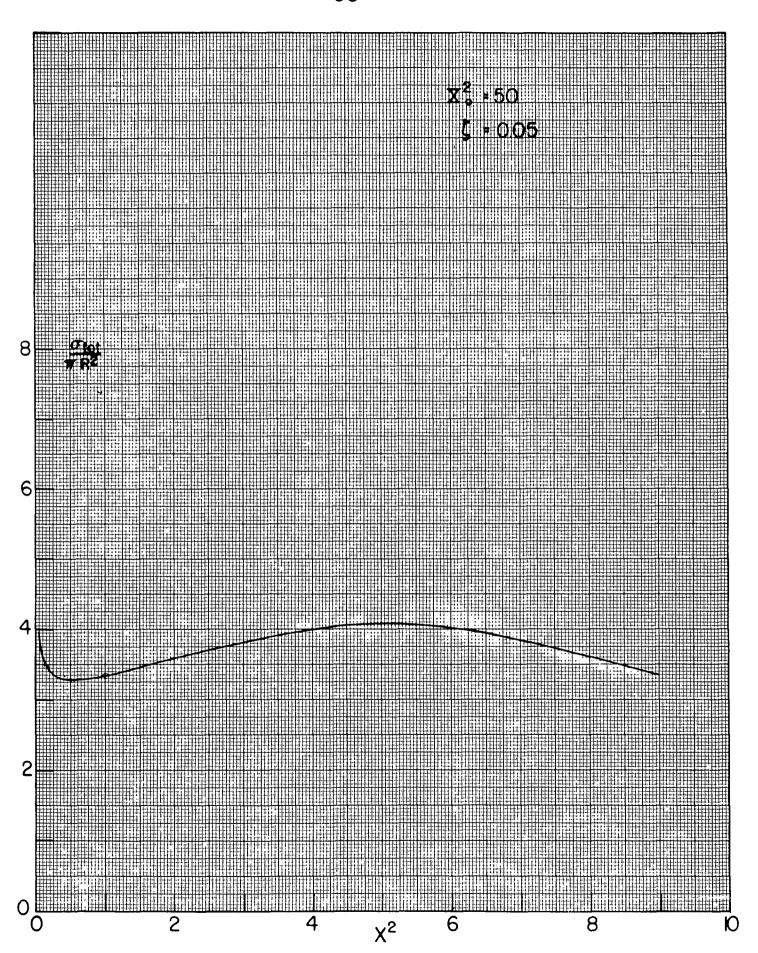


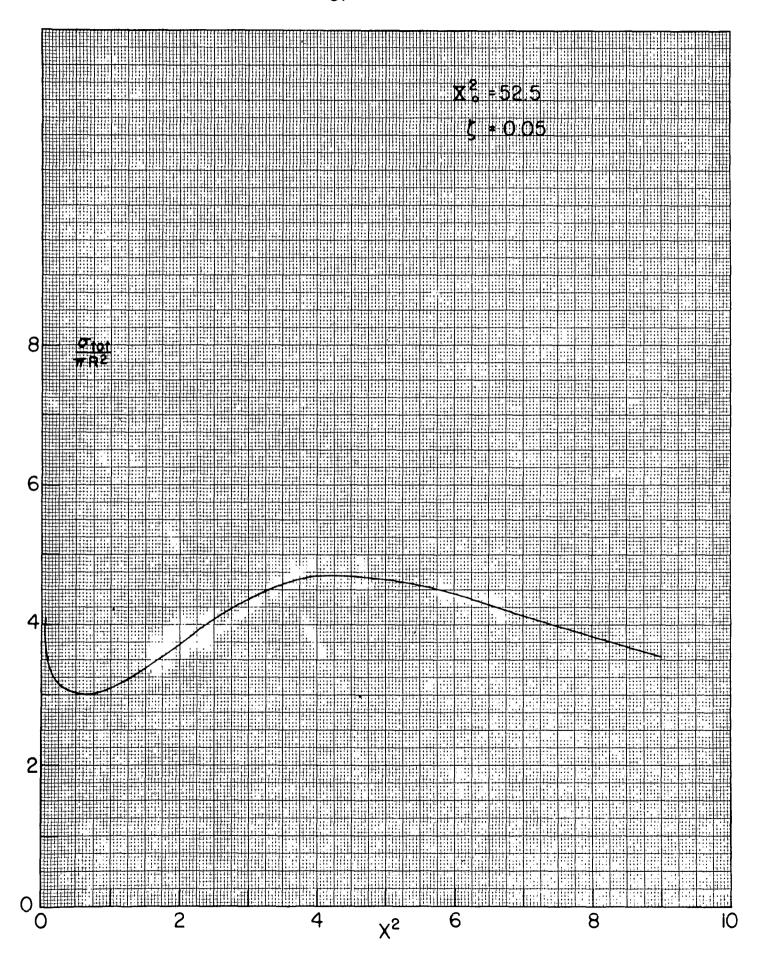


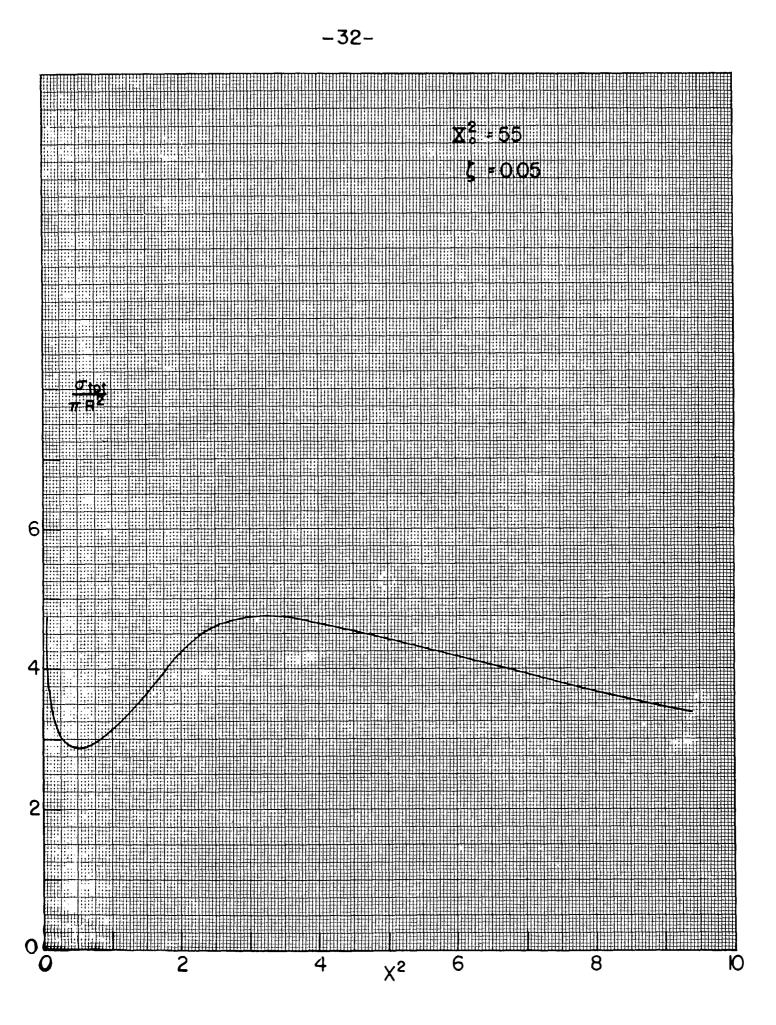


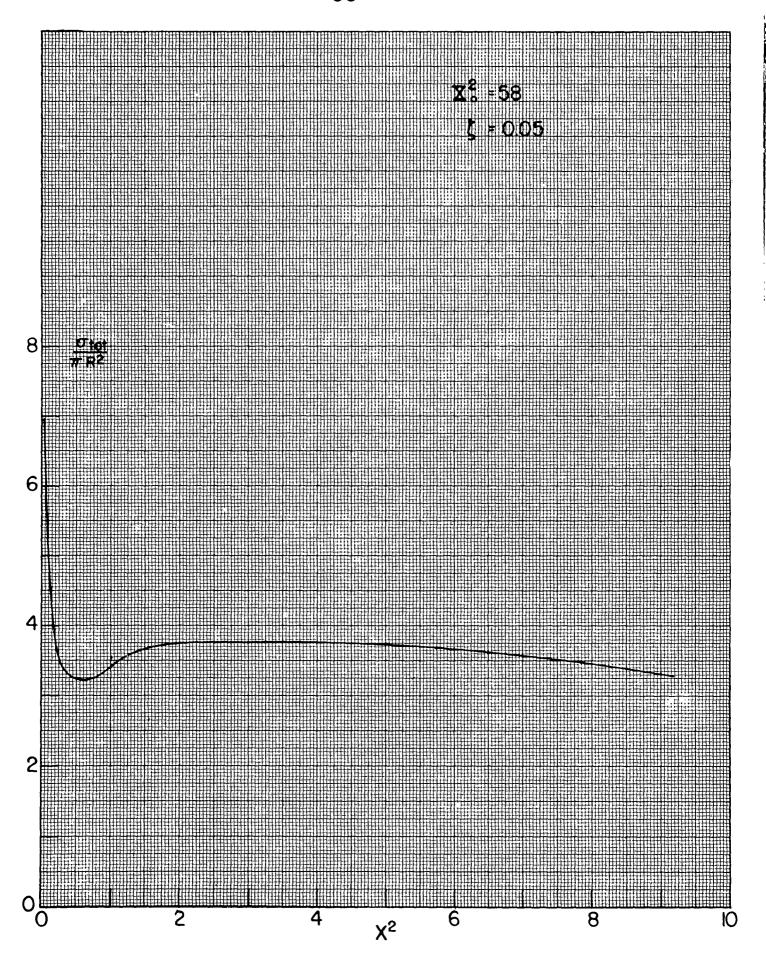


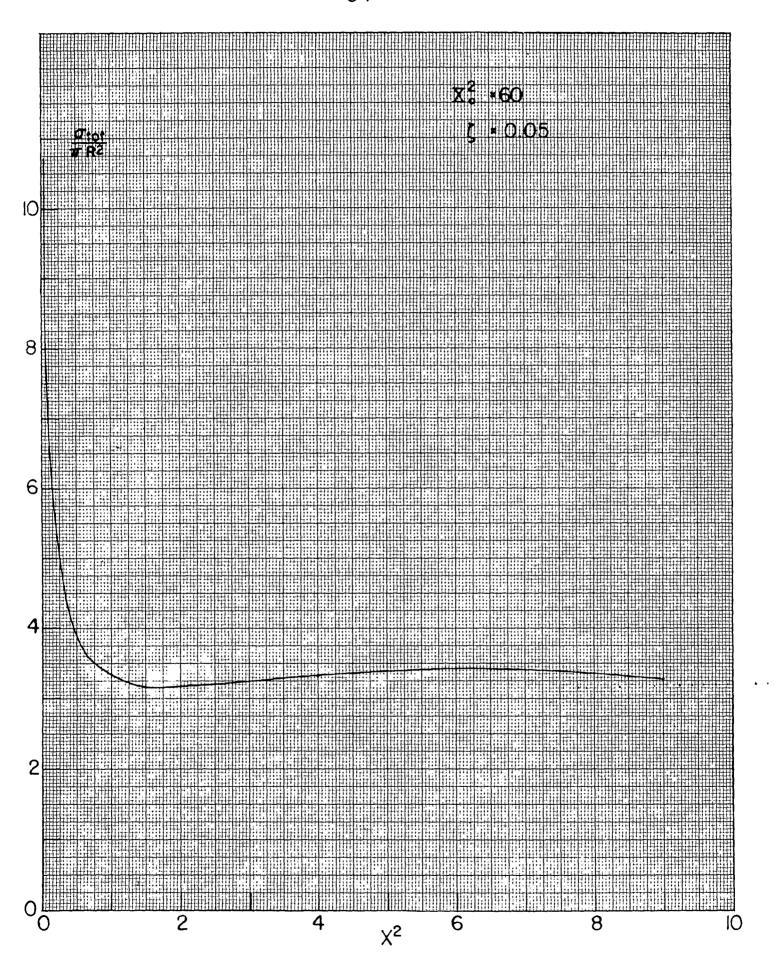


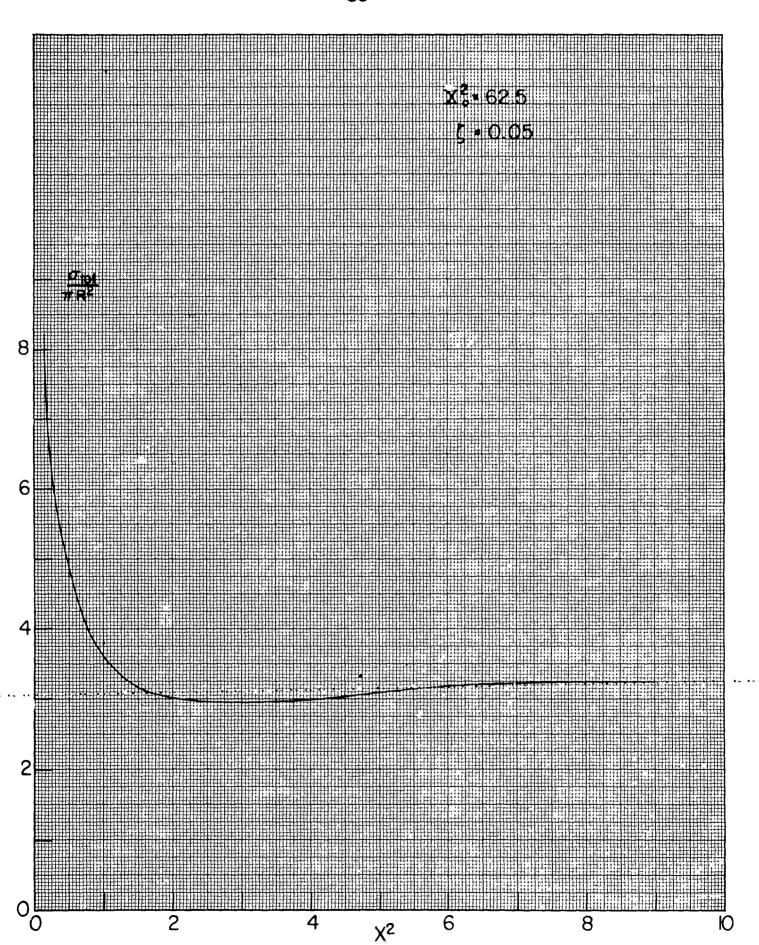


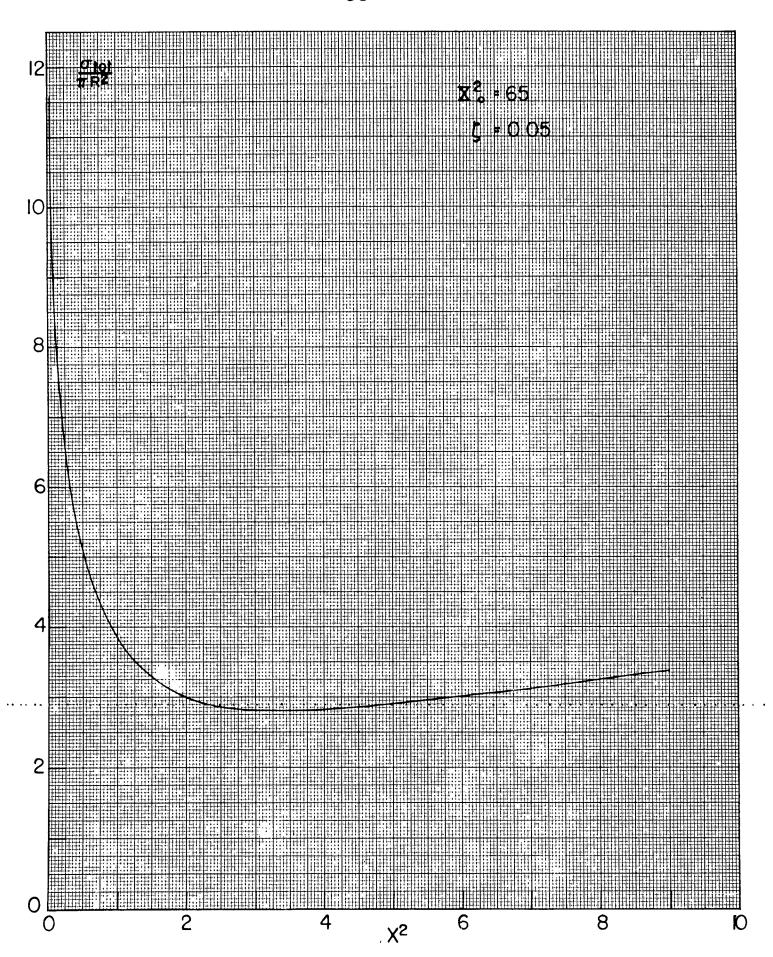


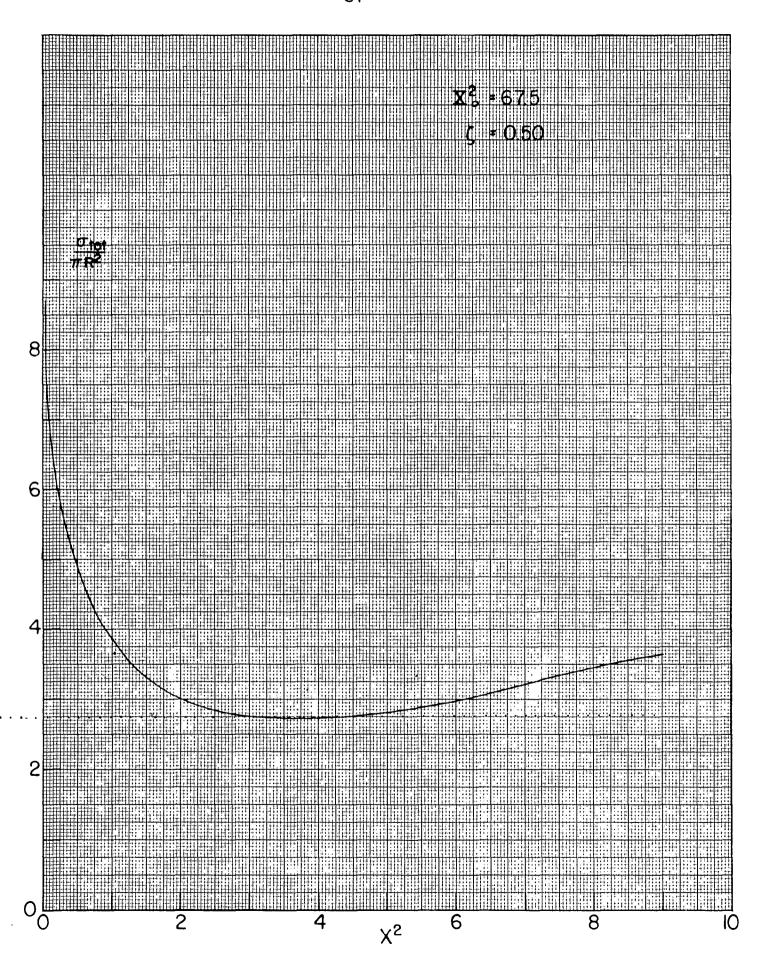


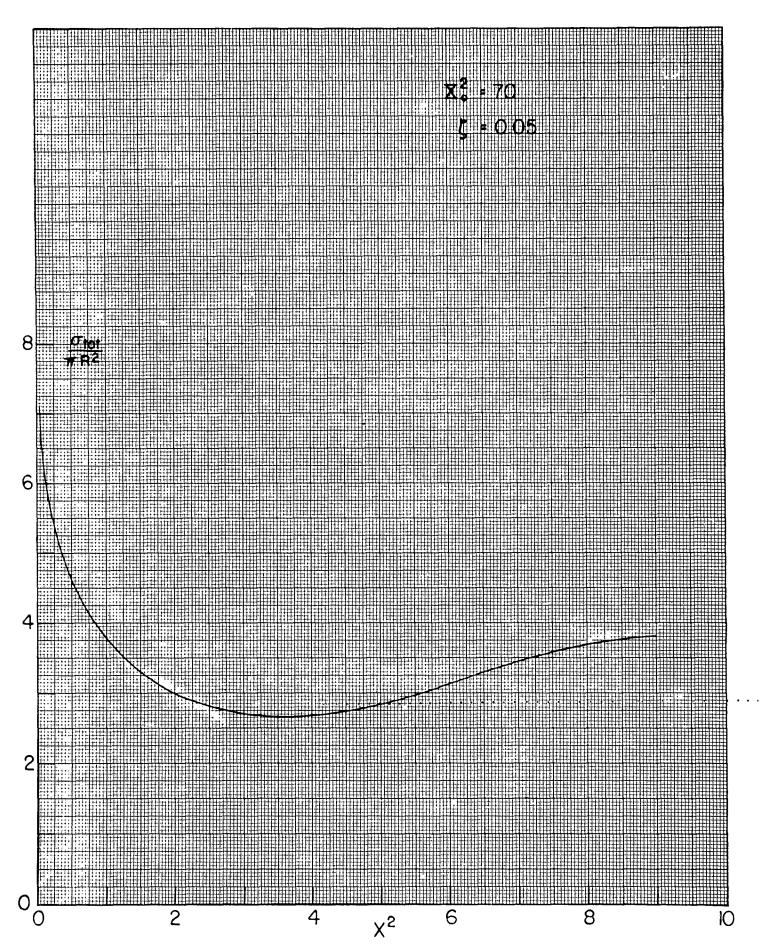


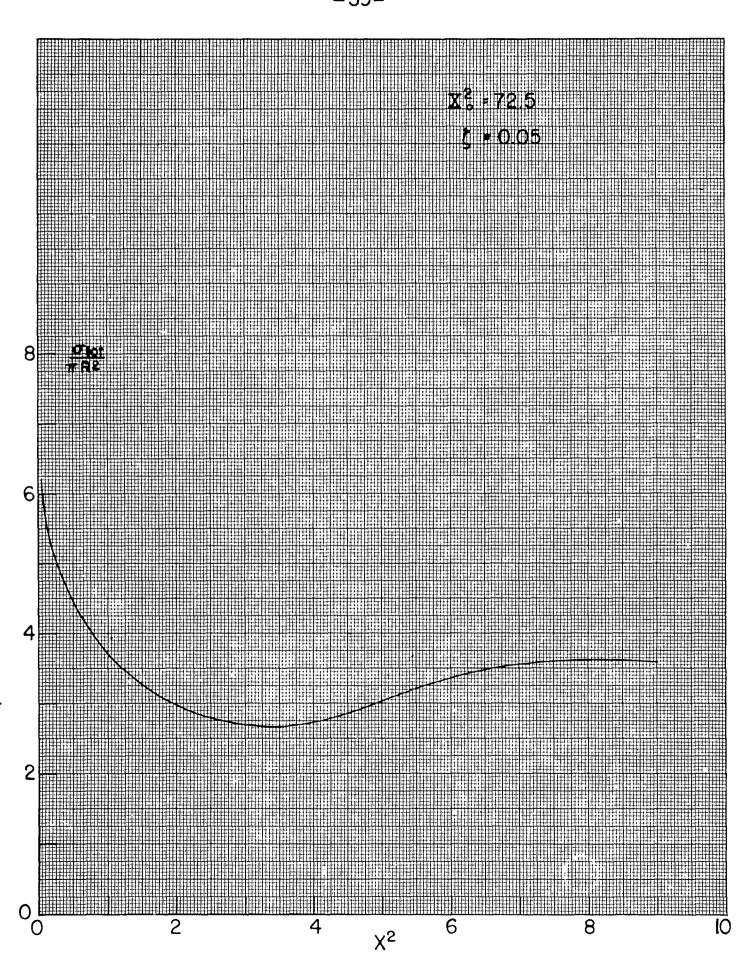




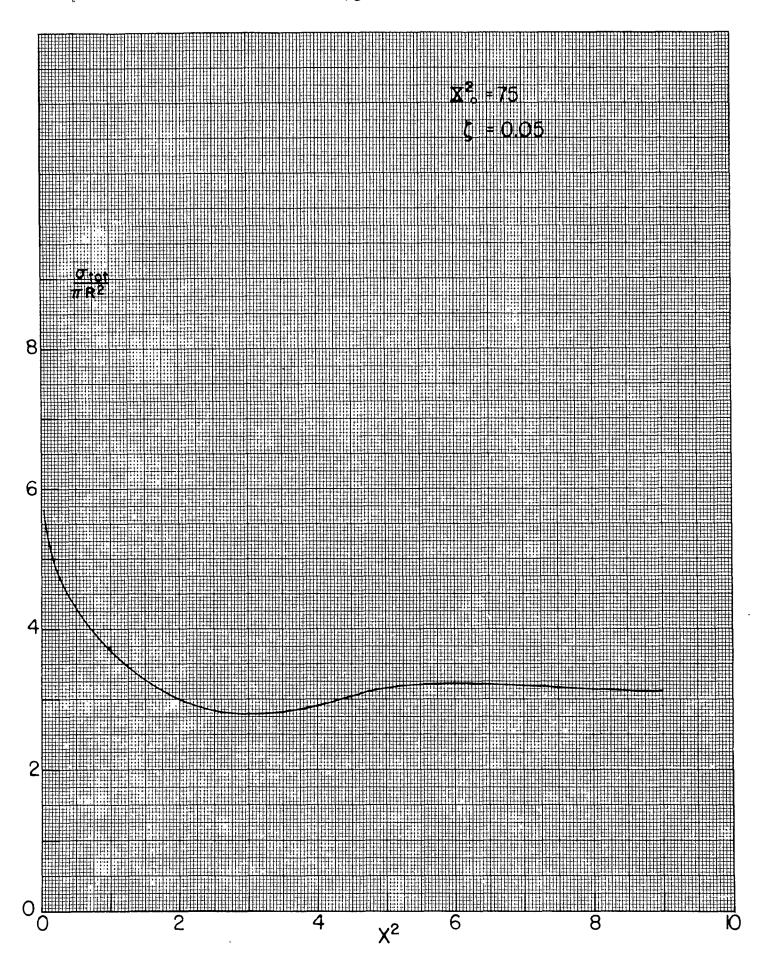


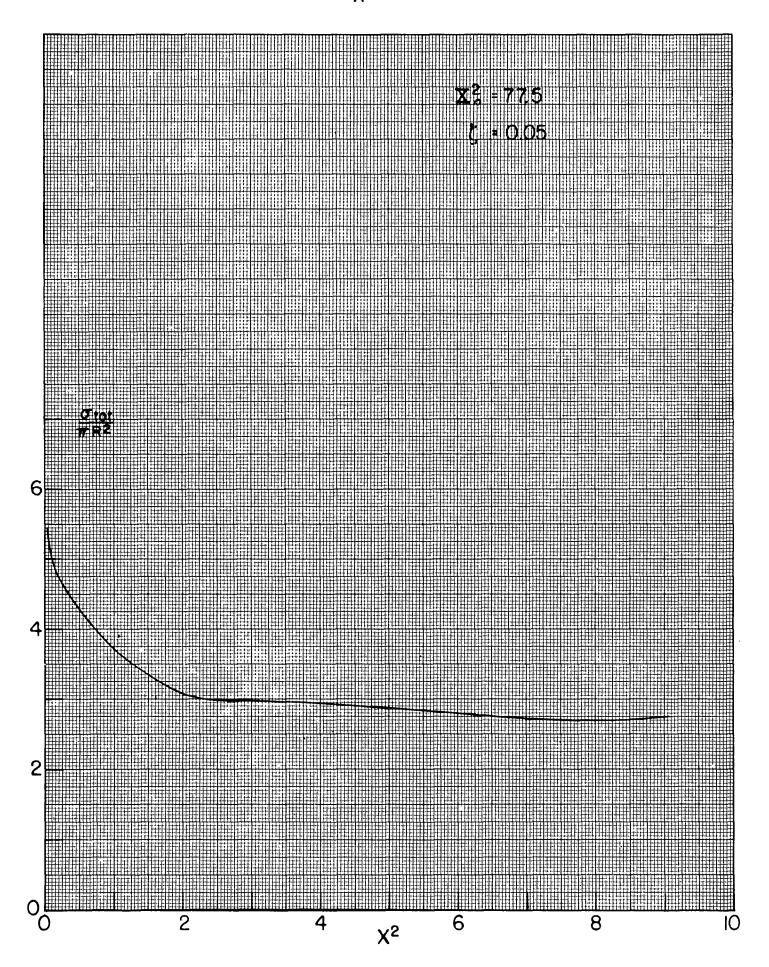


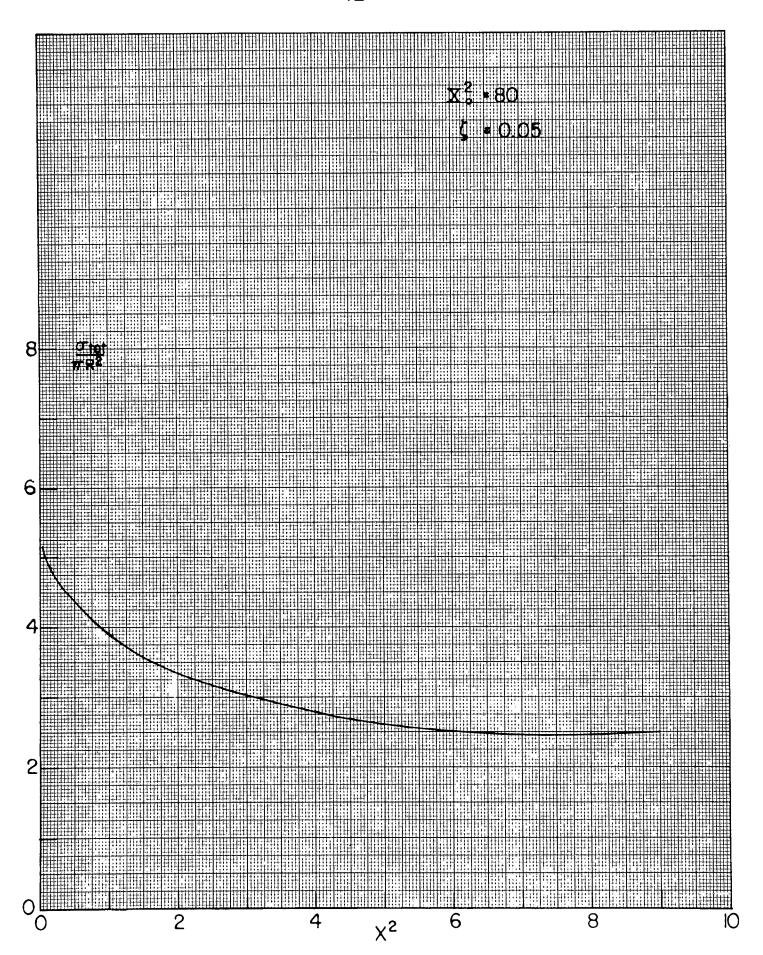




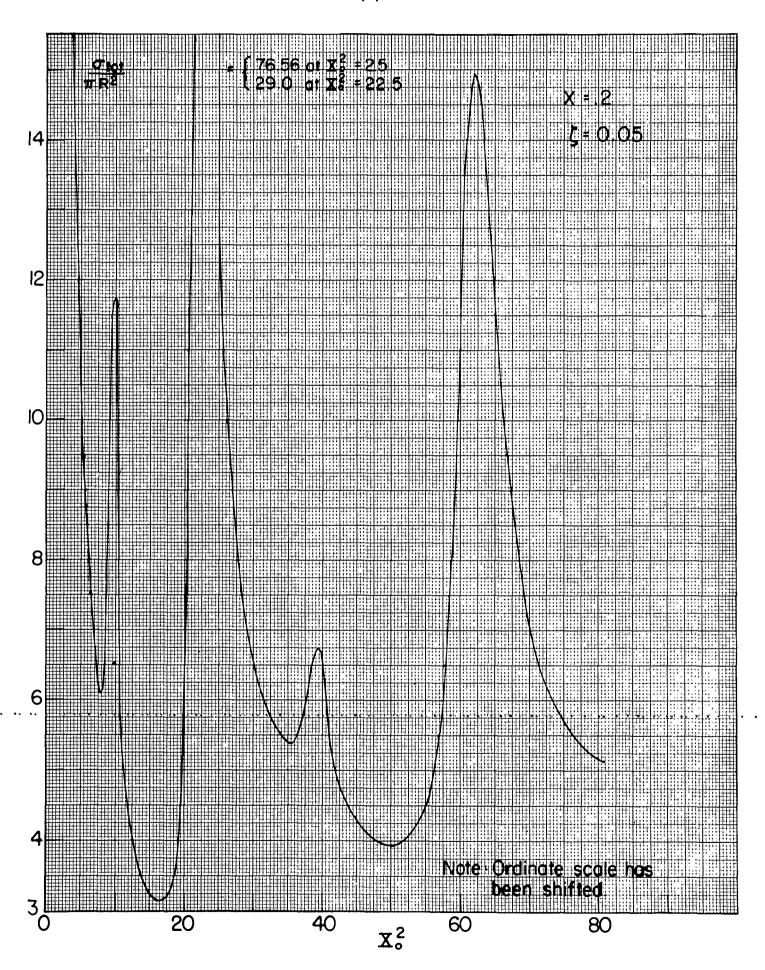
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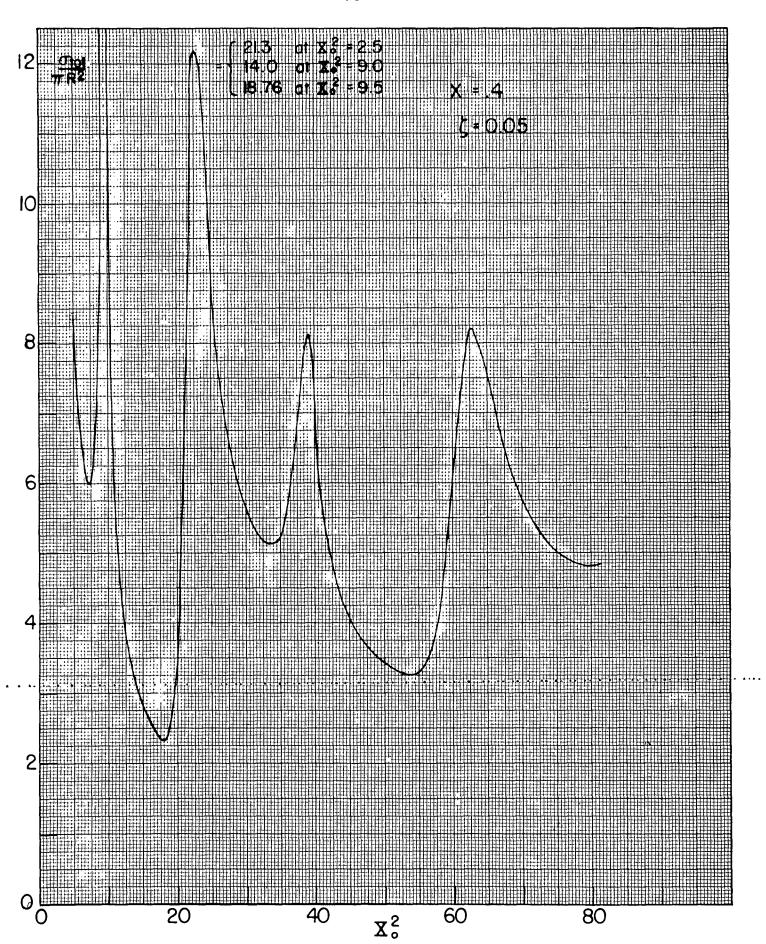


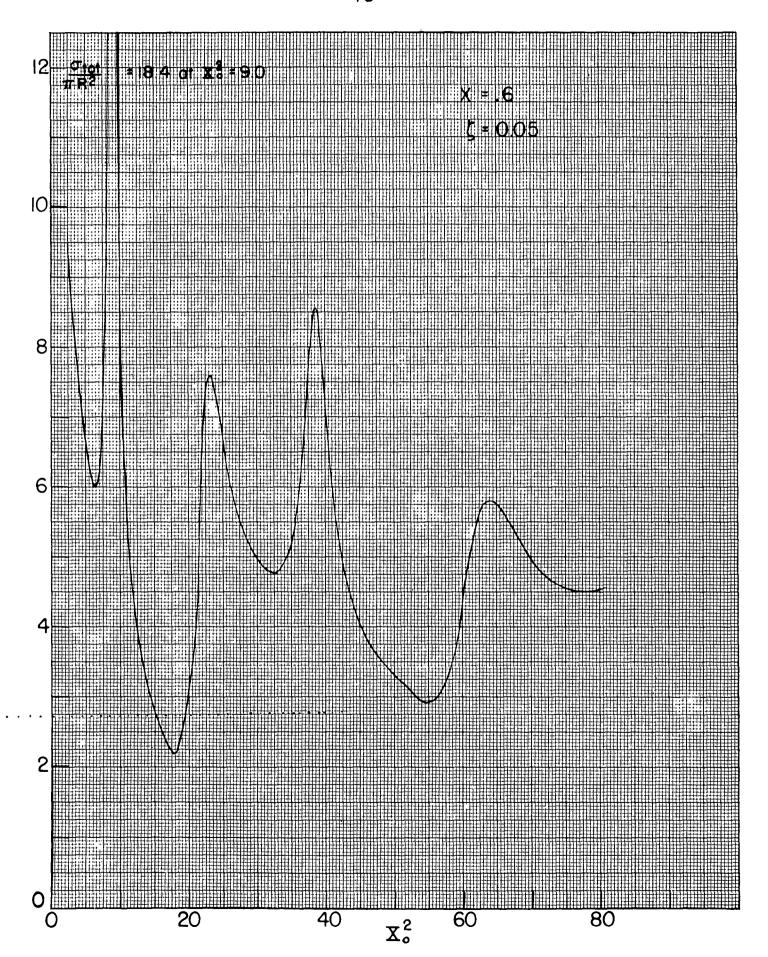


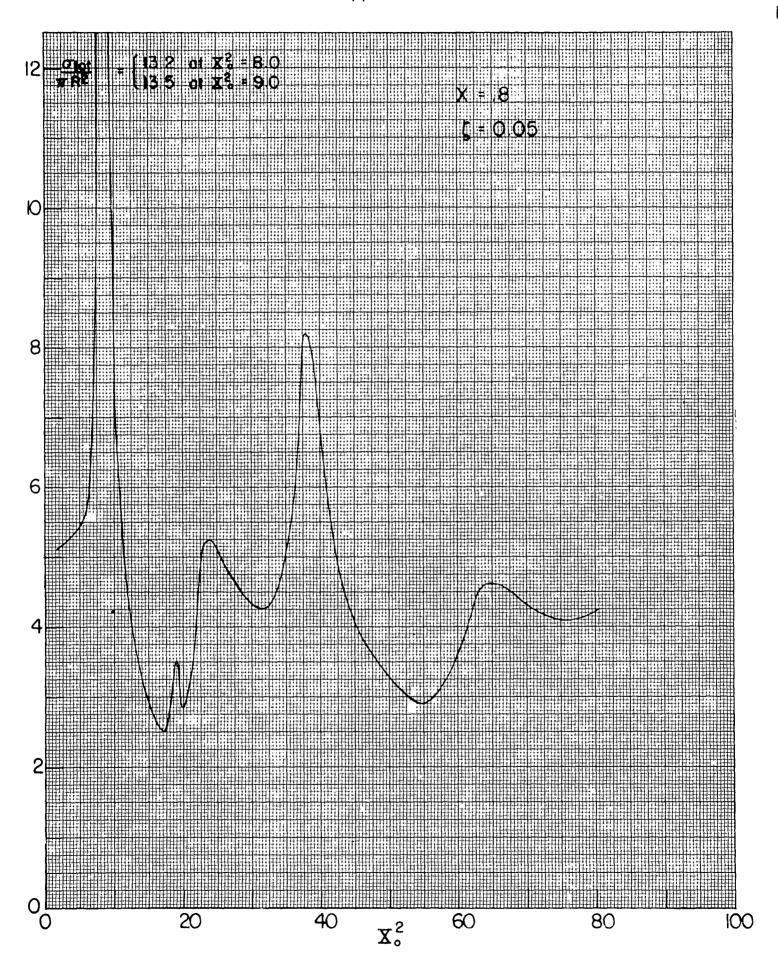


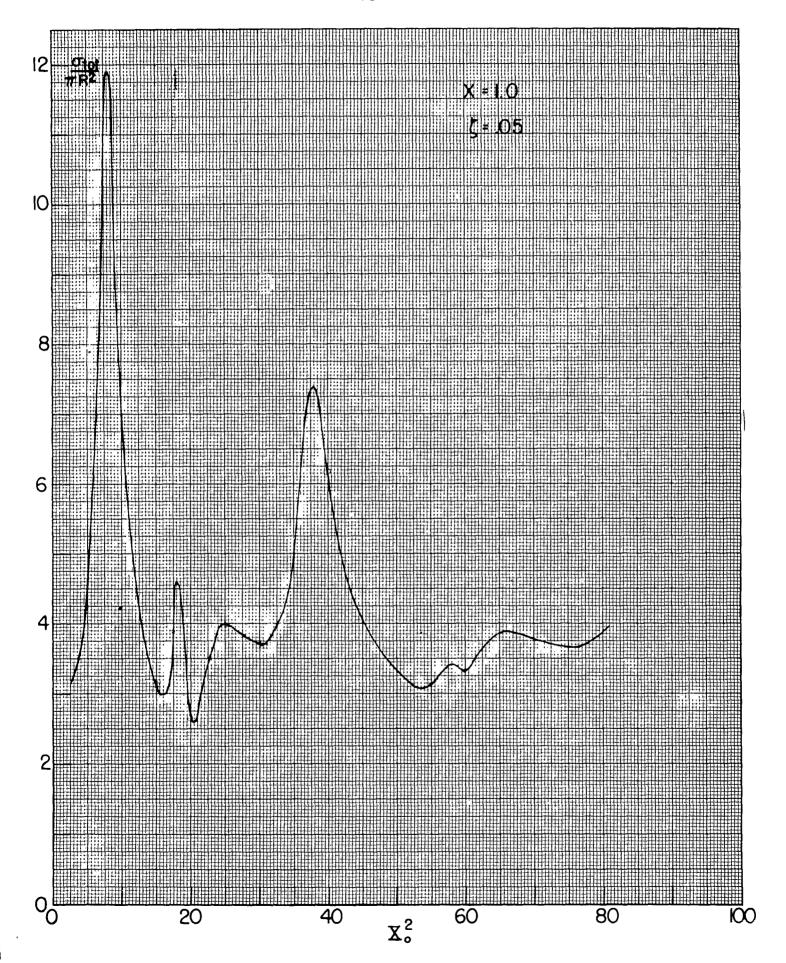
III. PLOTS OF TOTAL CROSS SECTION VS.  $x_0^2$  FOR FIXED  $x^2$  WITH  $\zeta = 0.05$ 

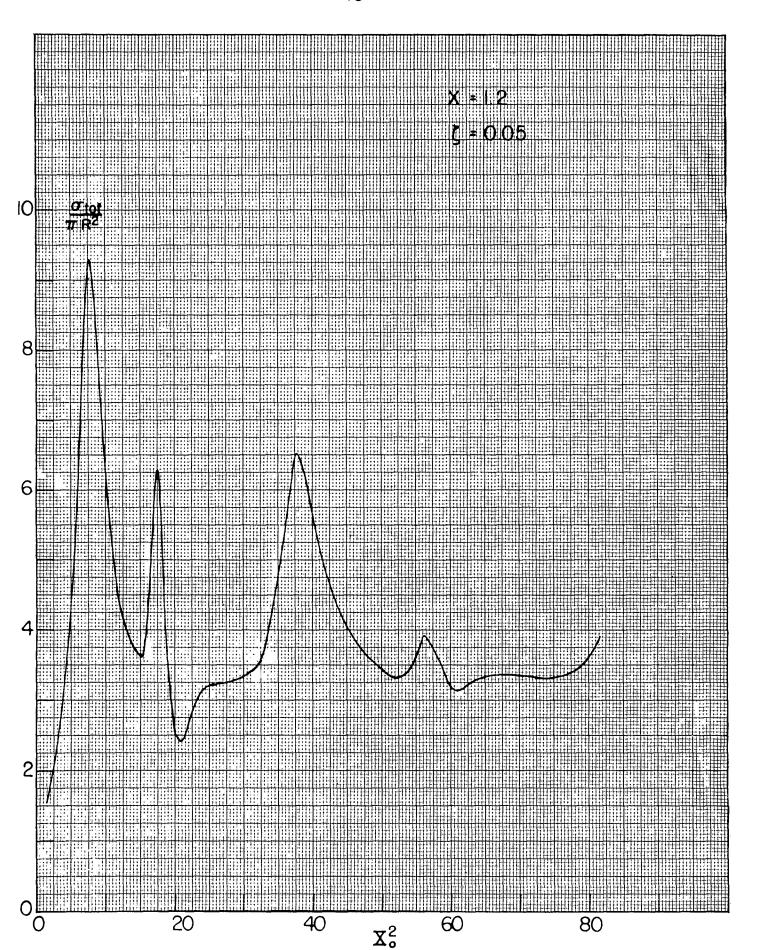


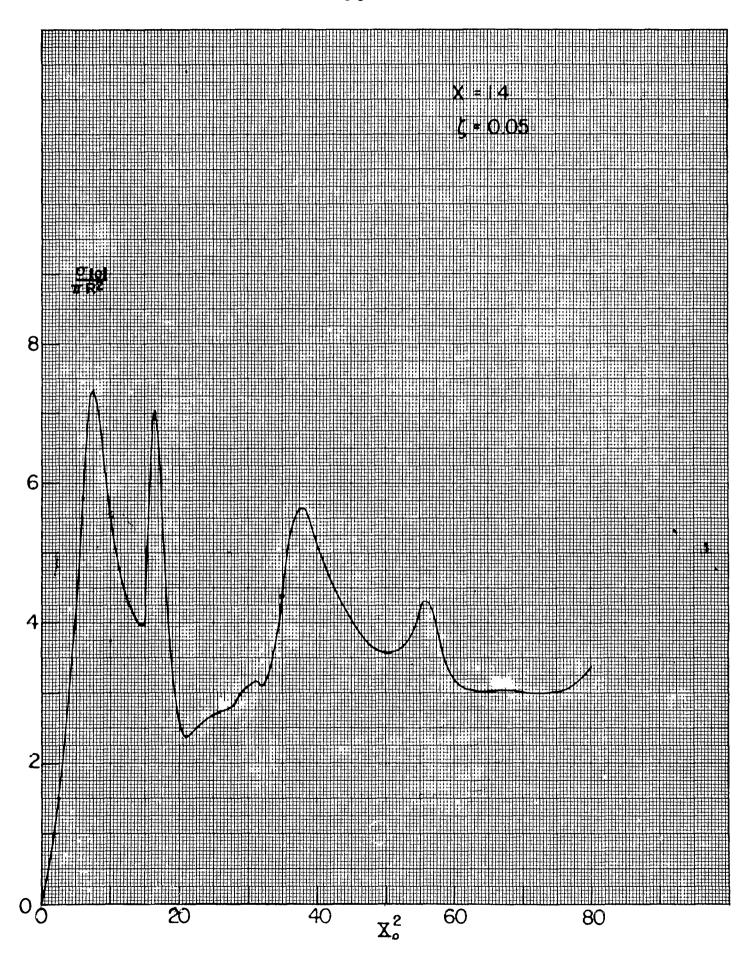


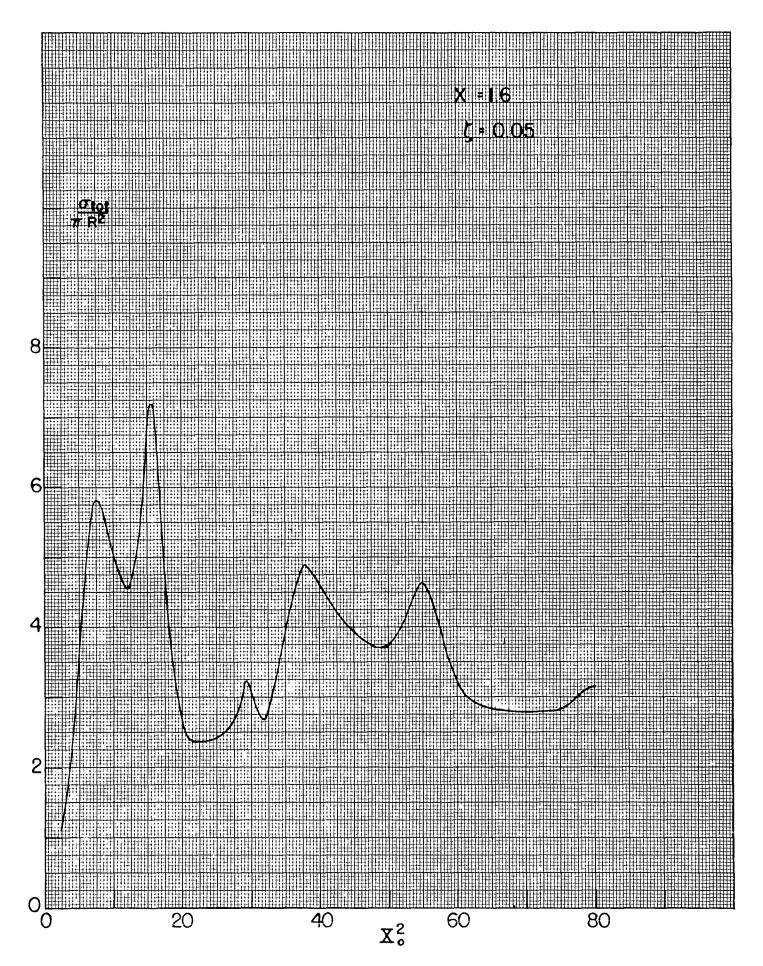


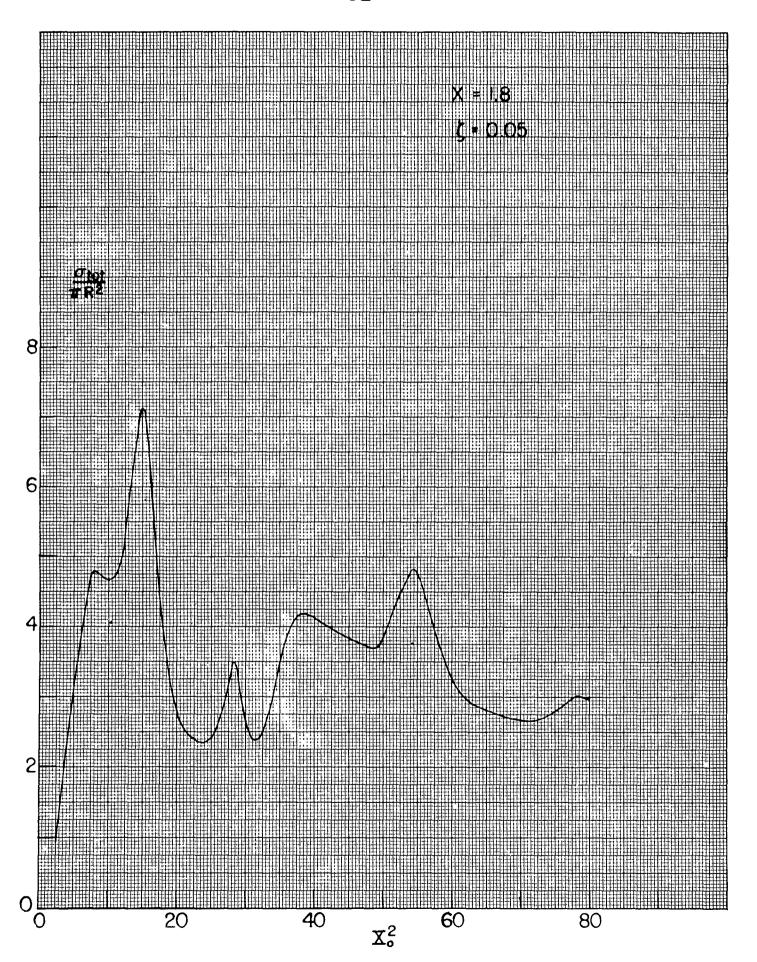


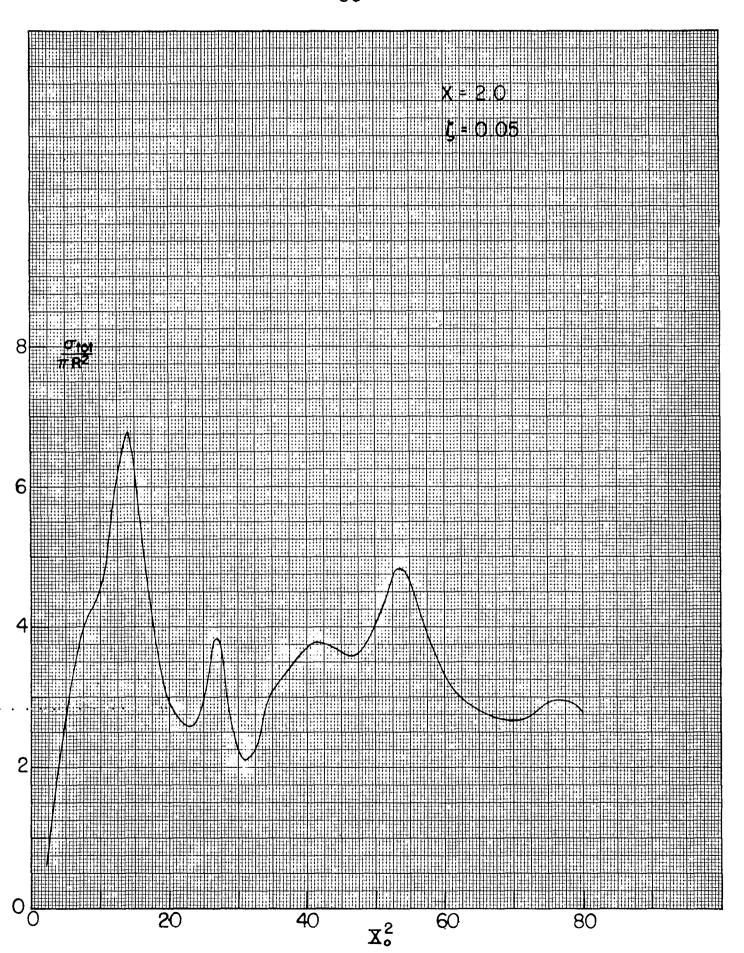


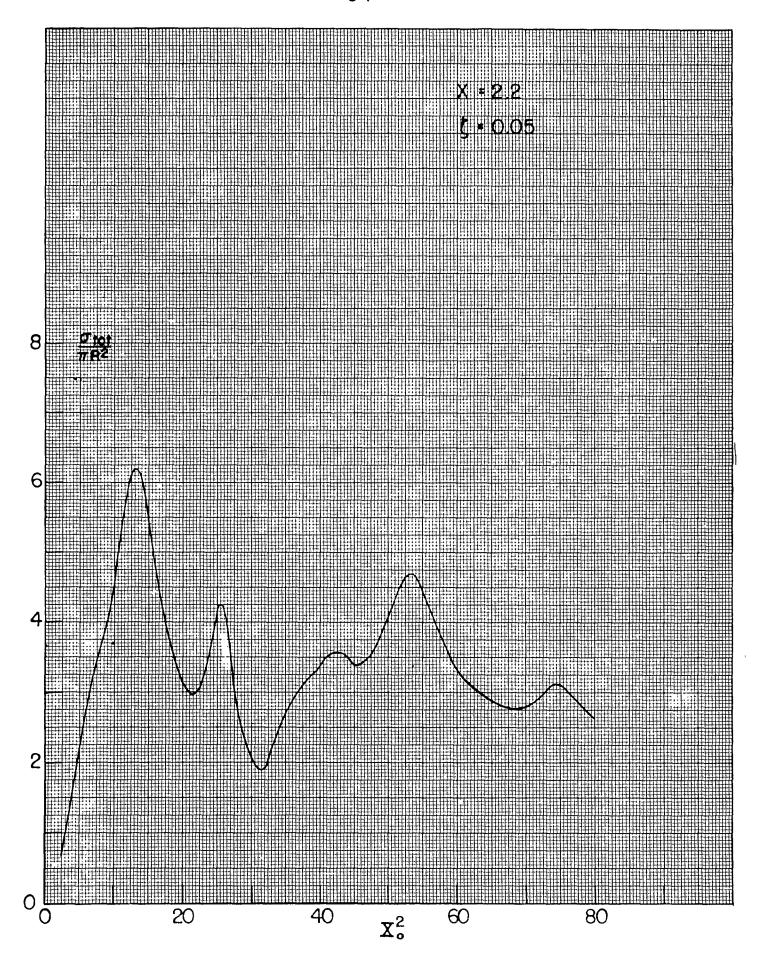


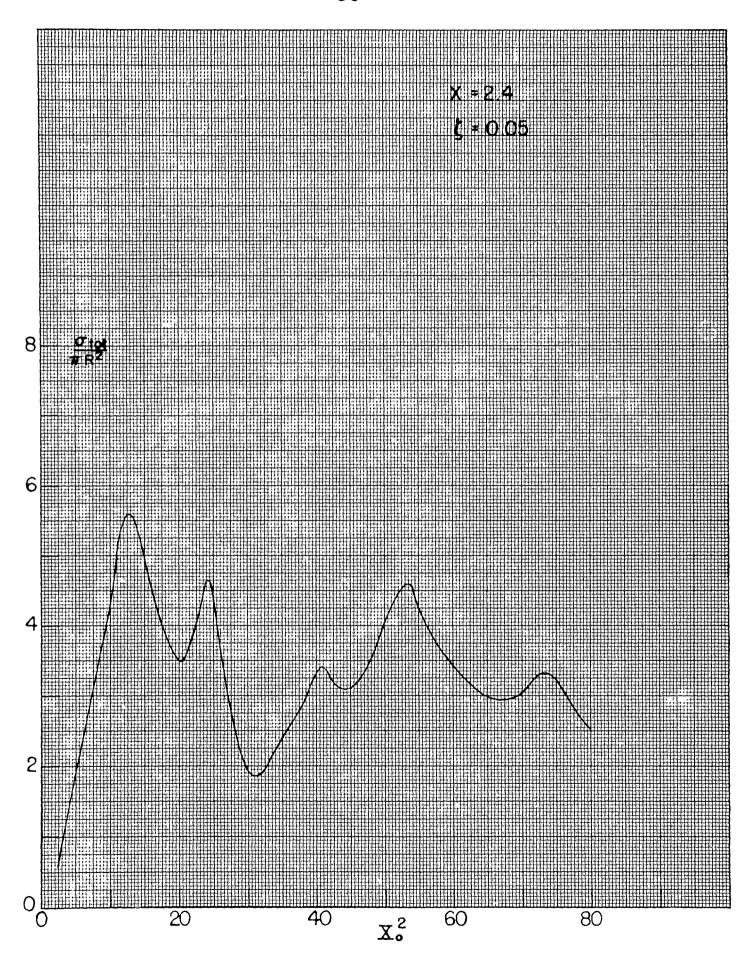


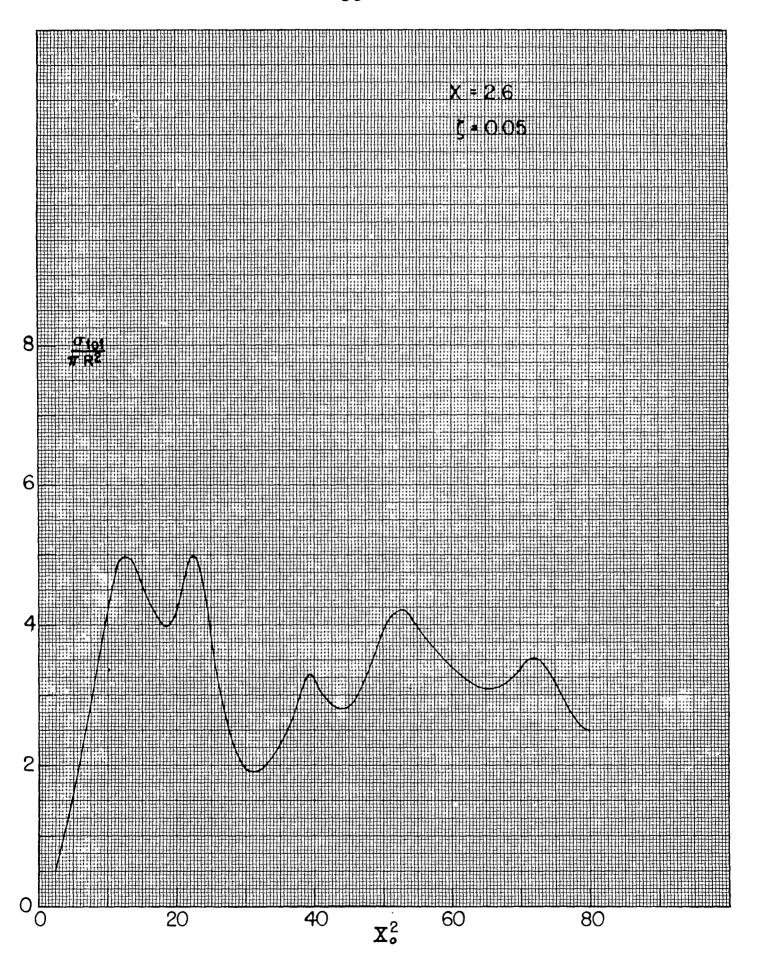


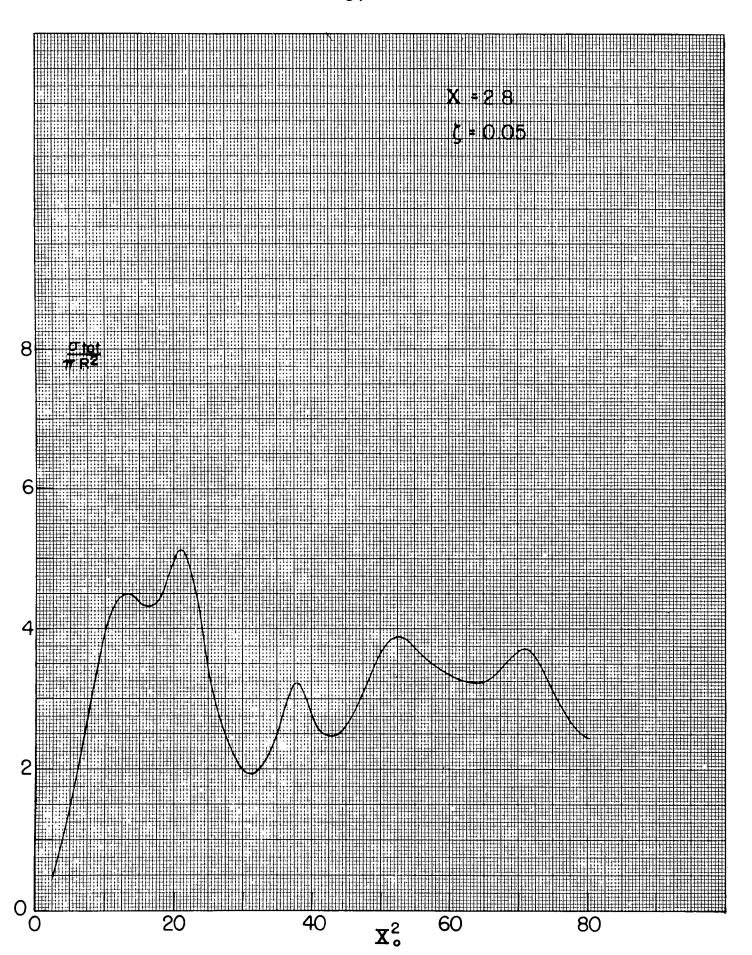


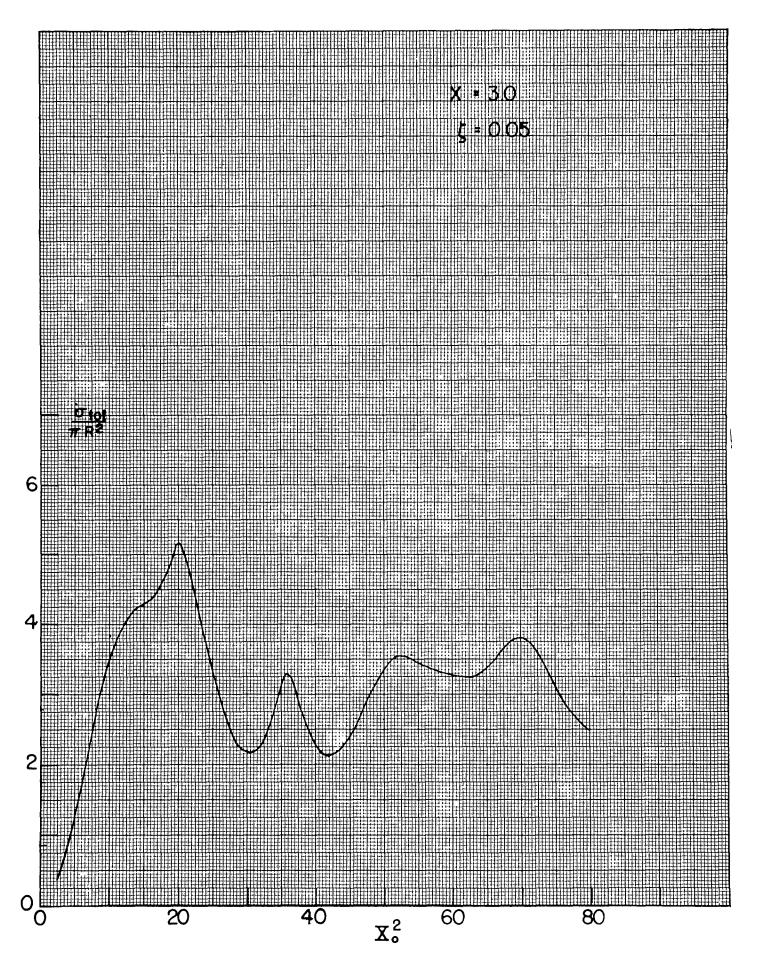






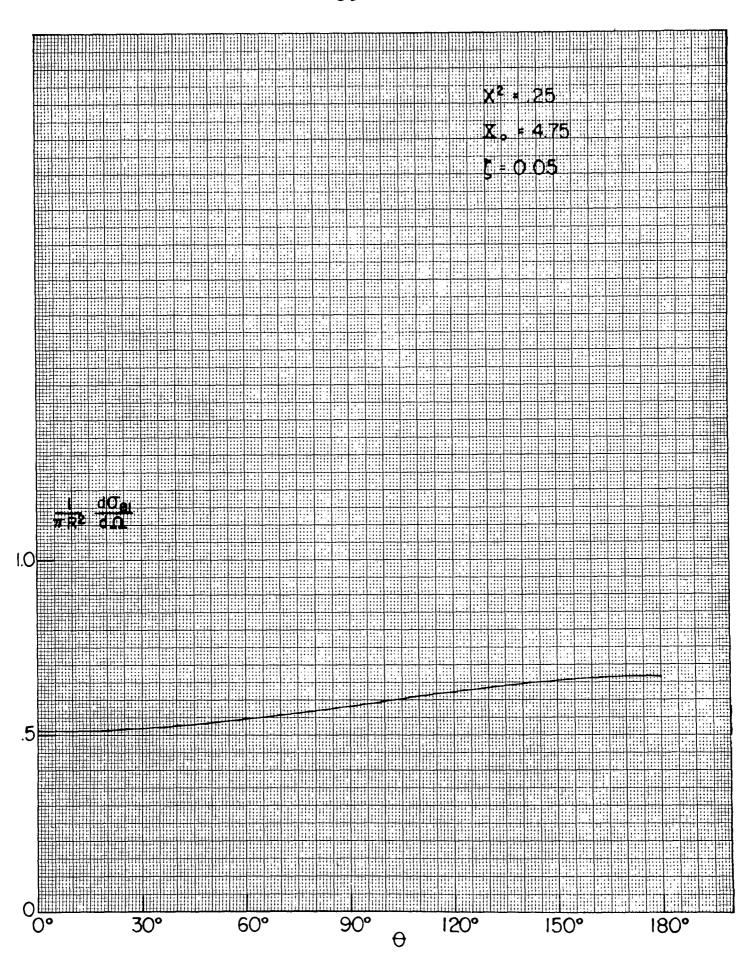


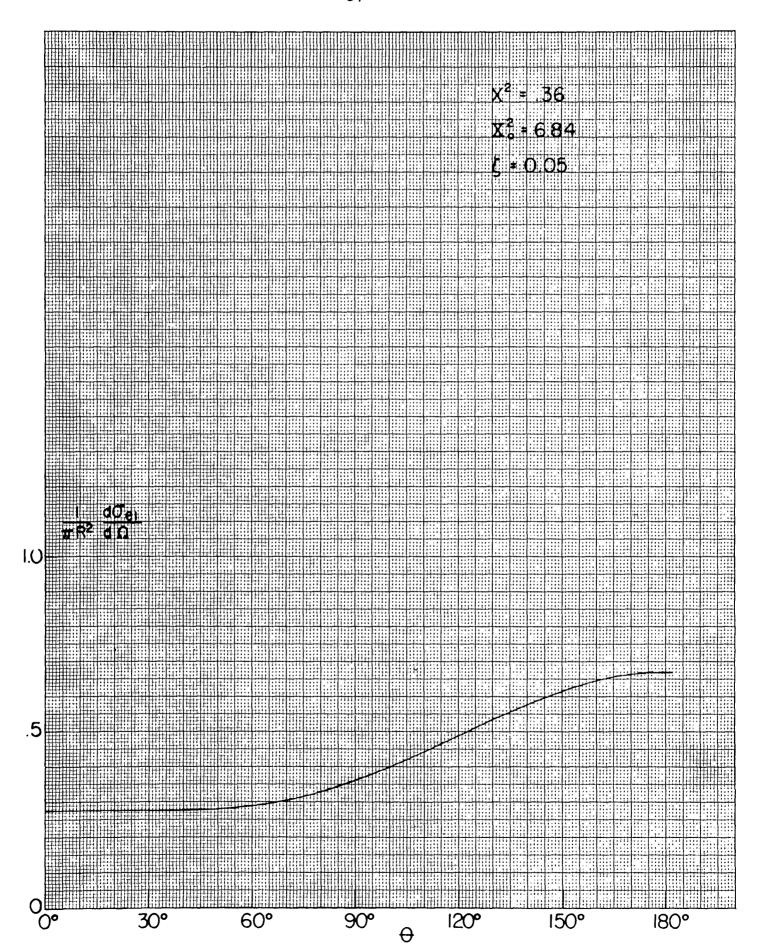


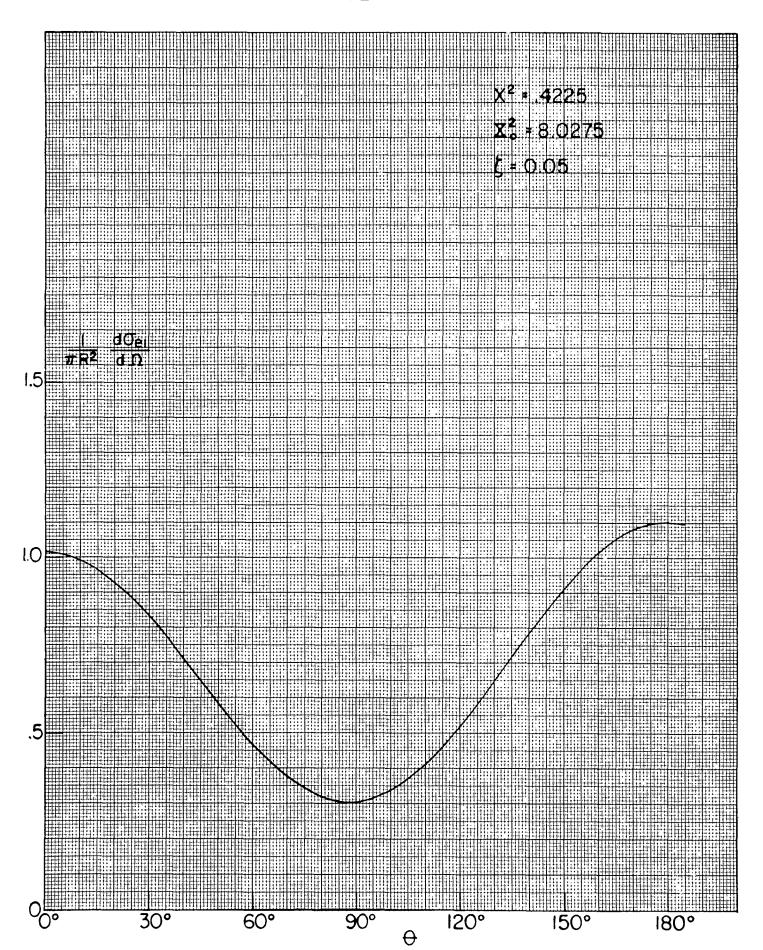


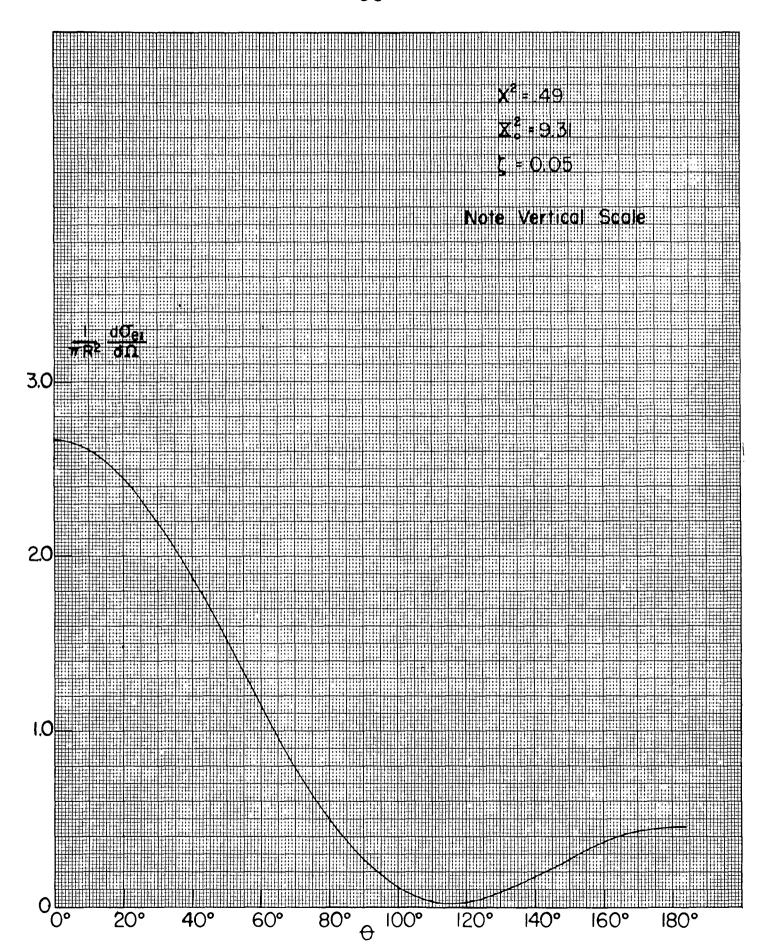
IV. PLOTS OF DIFFERENTIAL CROSS SECTION FOR ELASTIC SCATTERING (SHAPE-ELASTIC ONLY)

FOR  $x^2/x_0^2 = 1/19$  WITH  $\xi = 0.05$ 

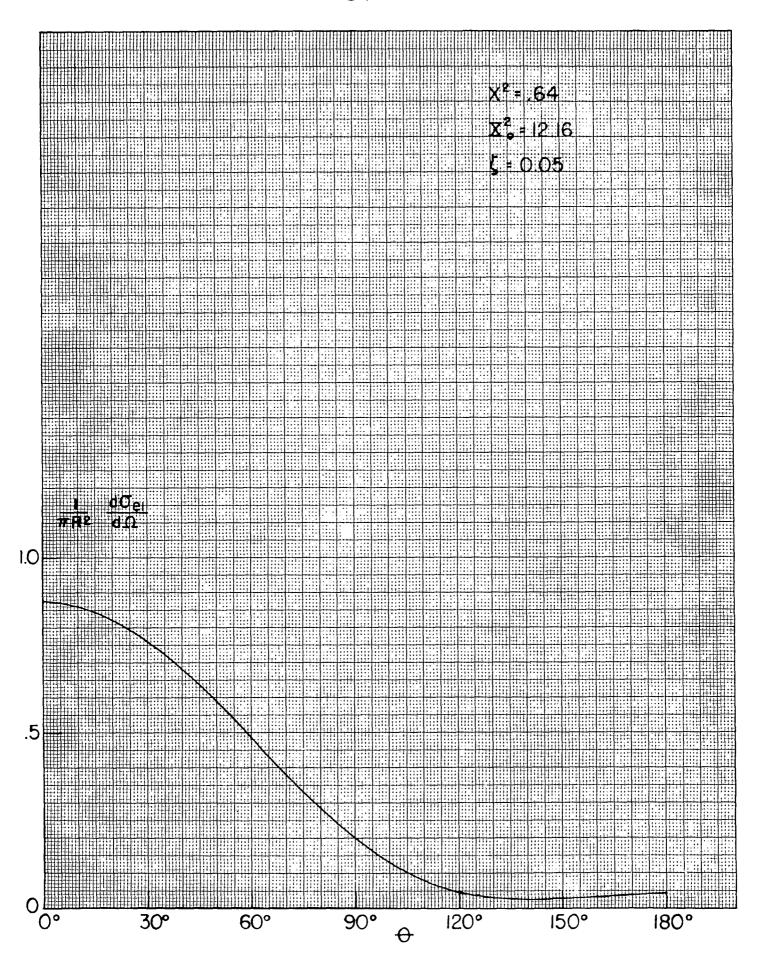


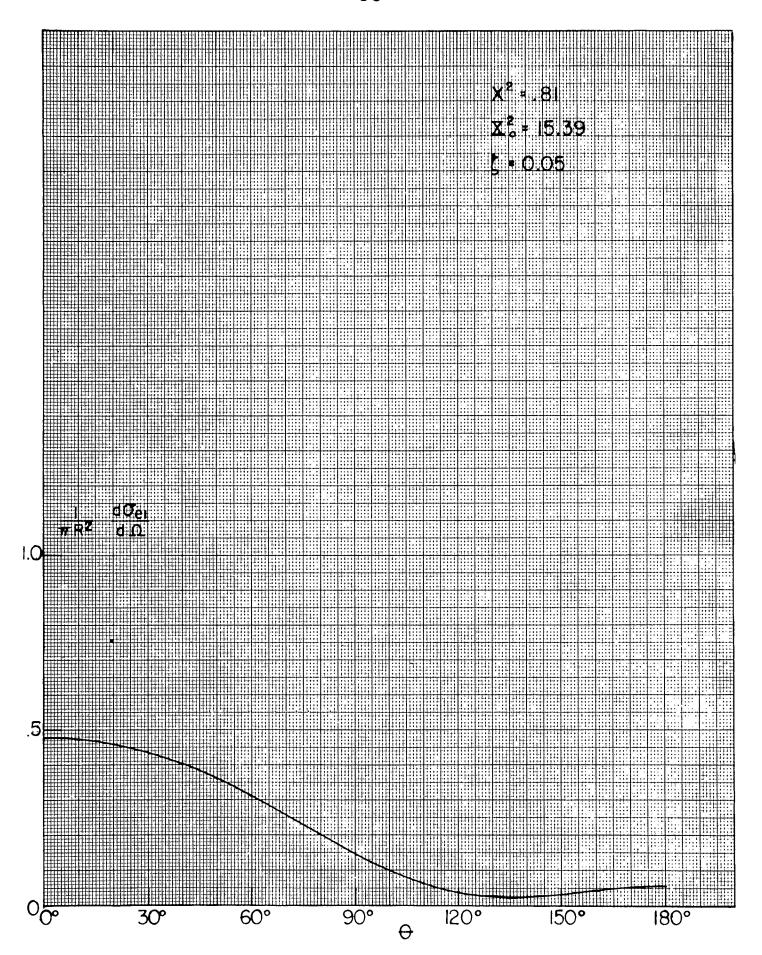


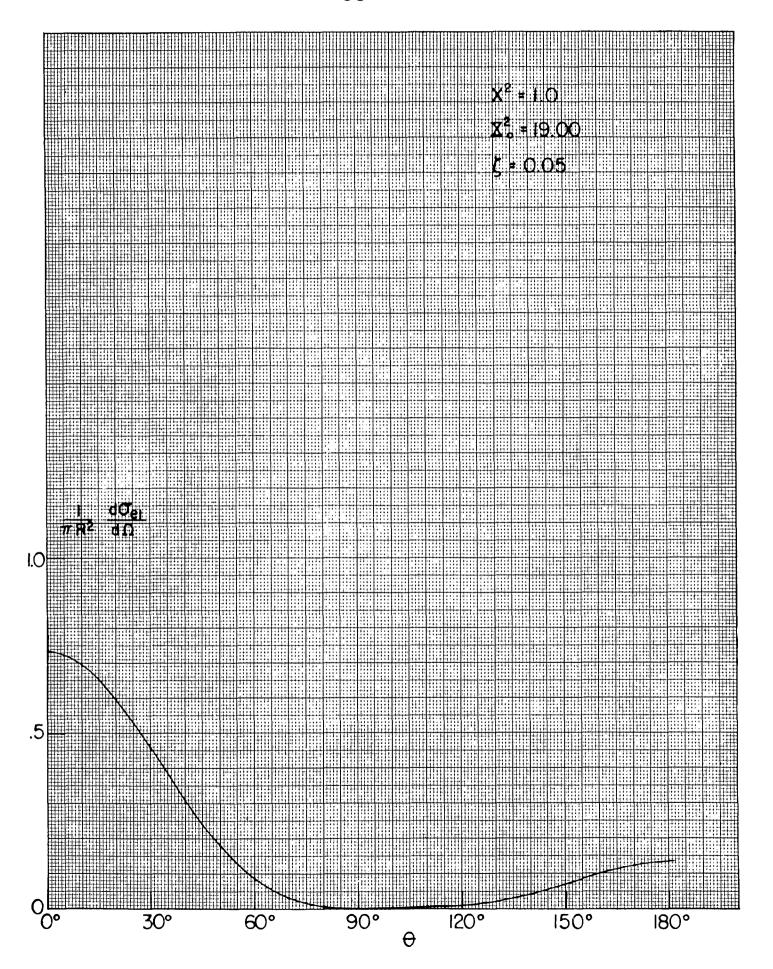


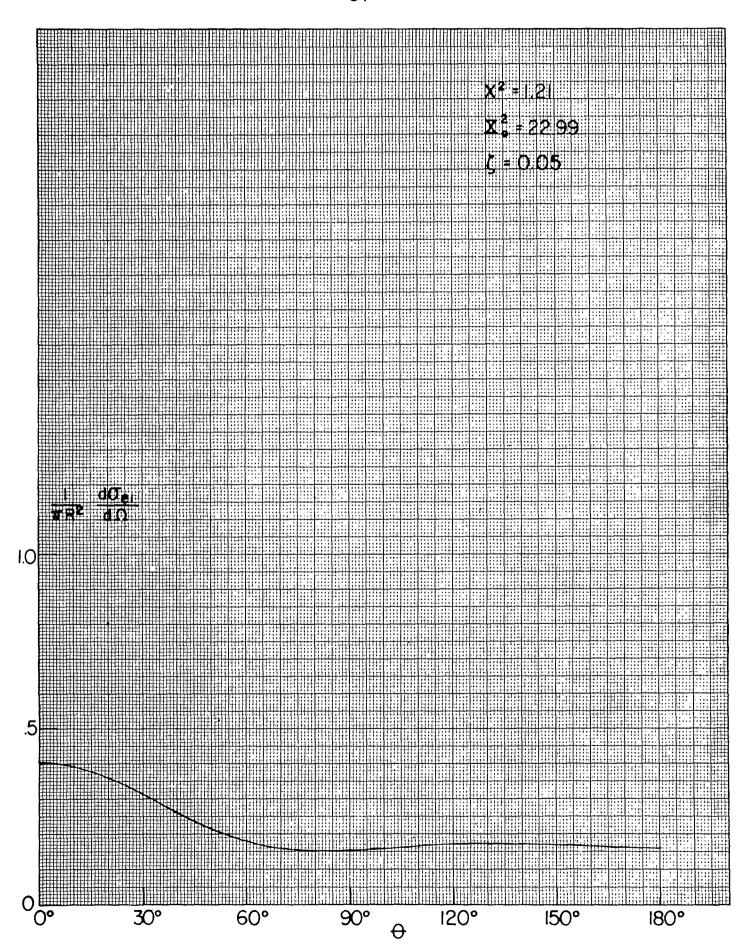


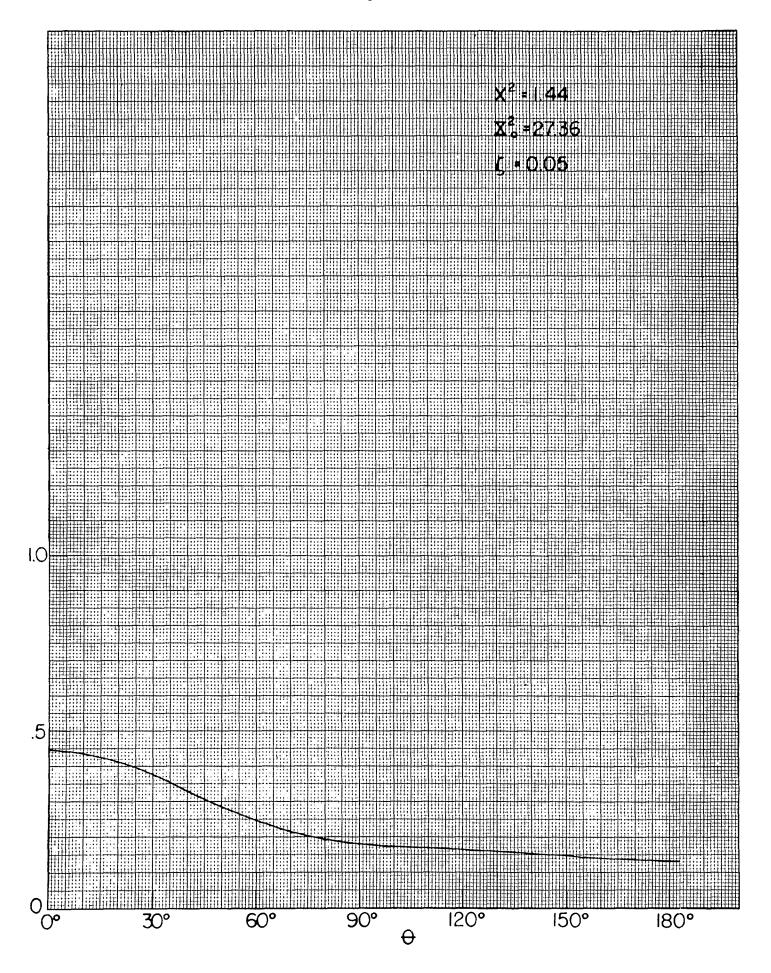
E X



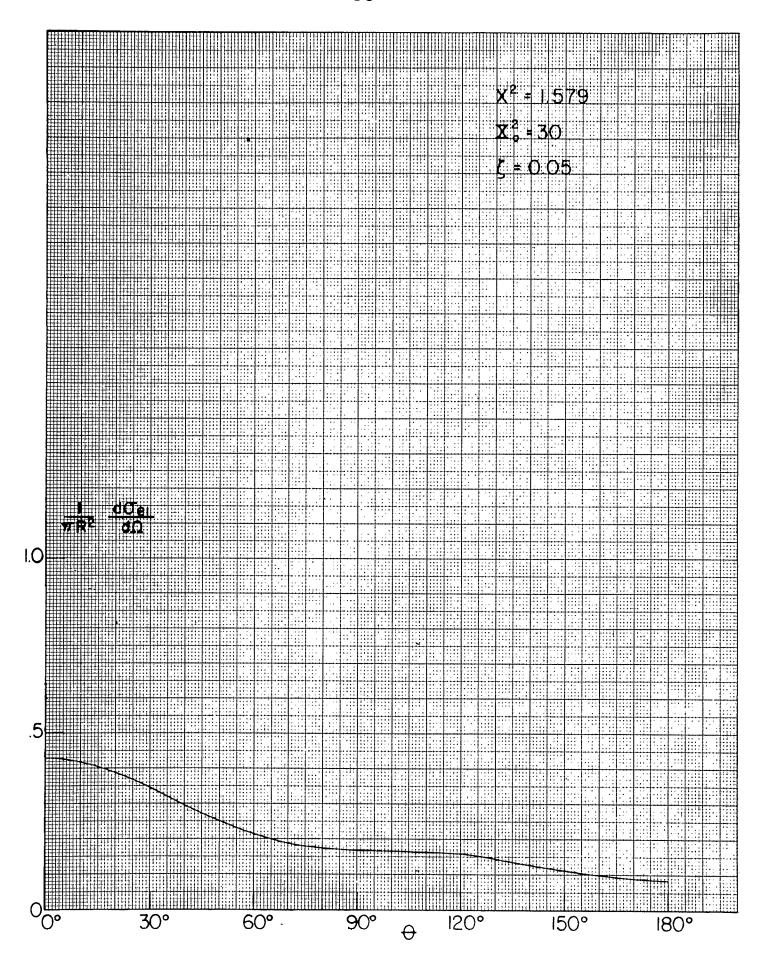




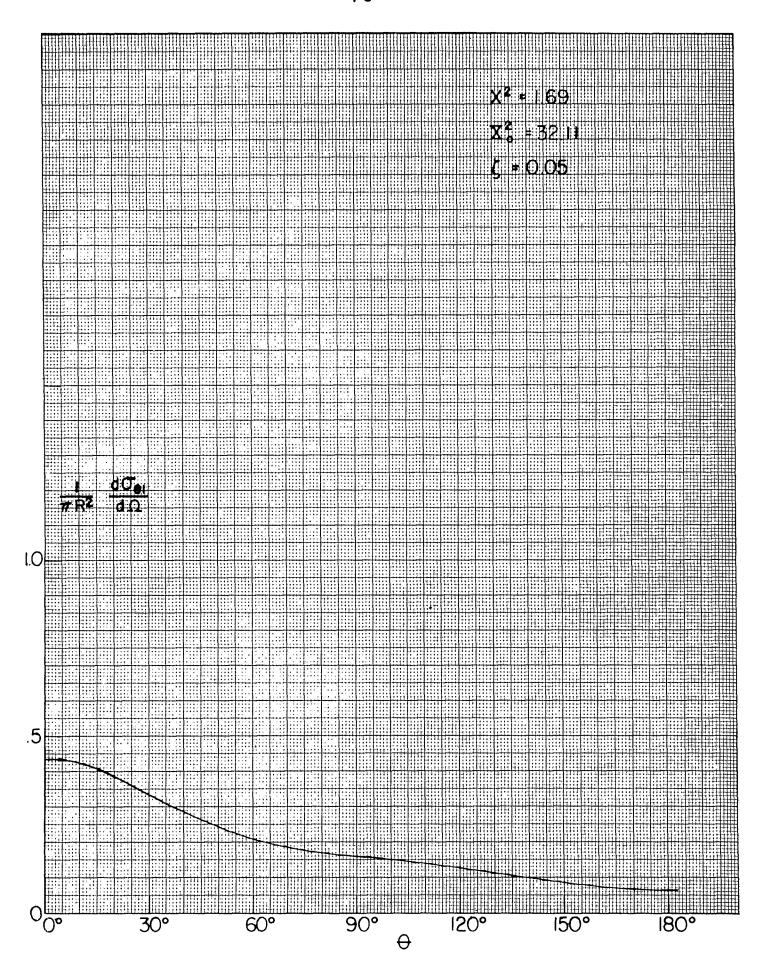


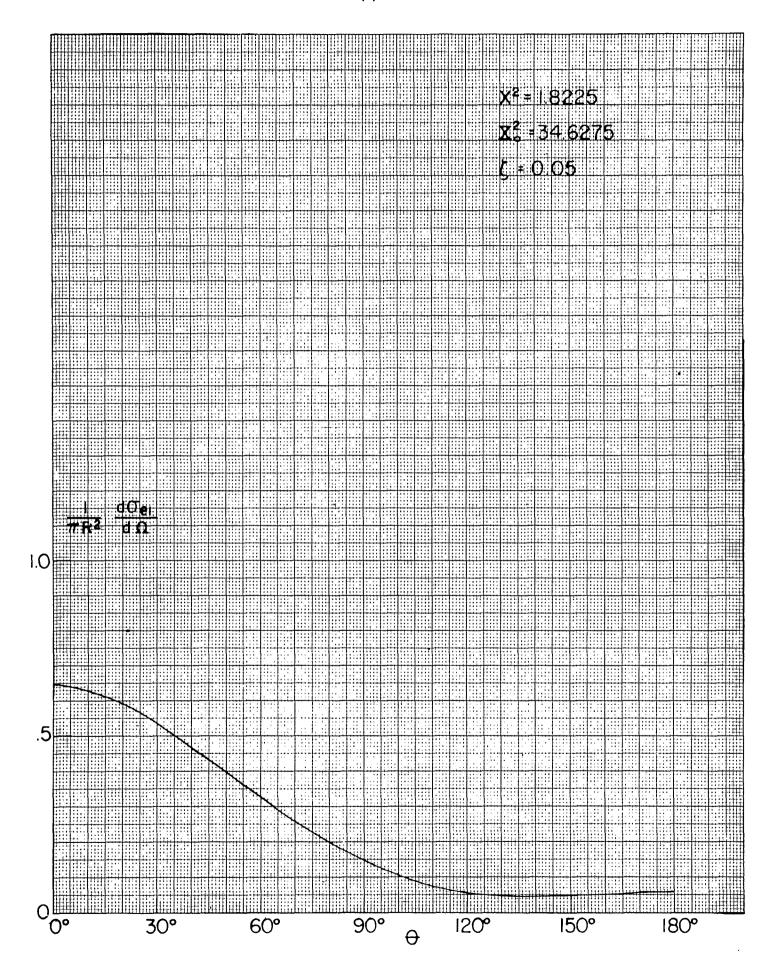


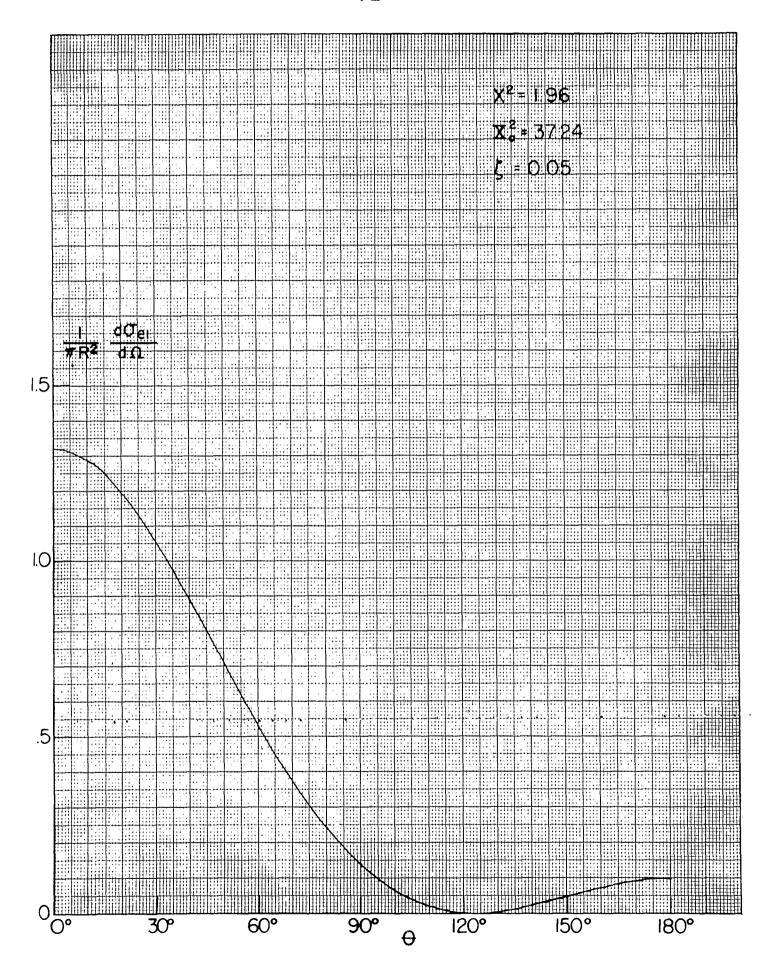
E XX

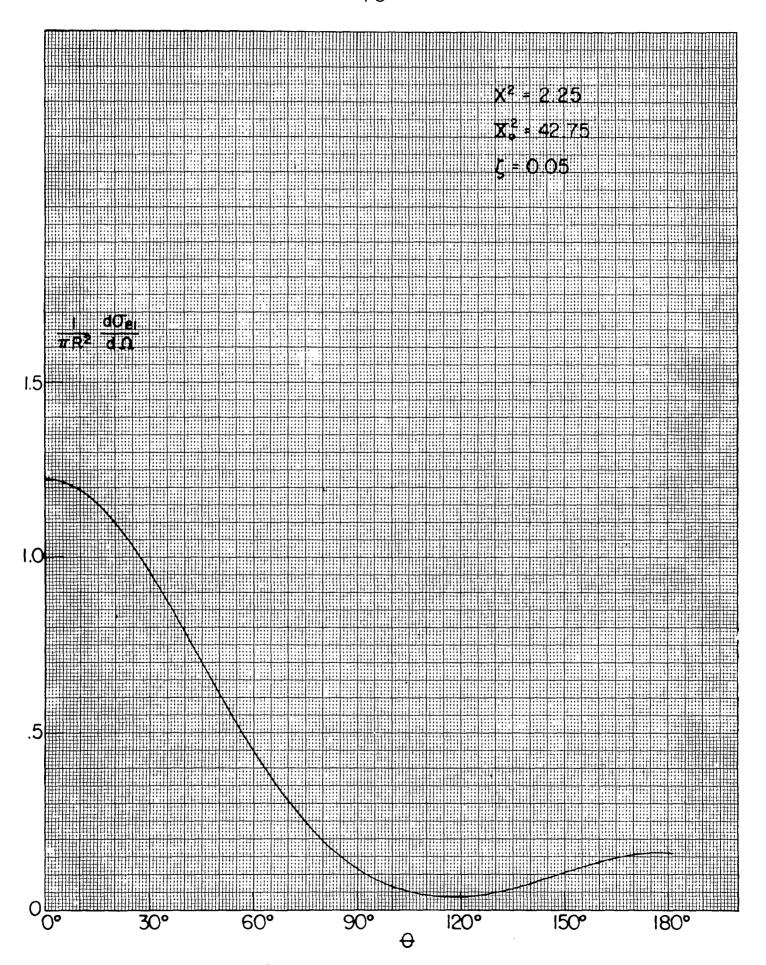


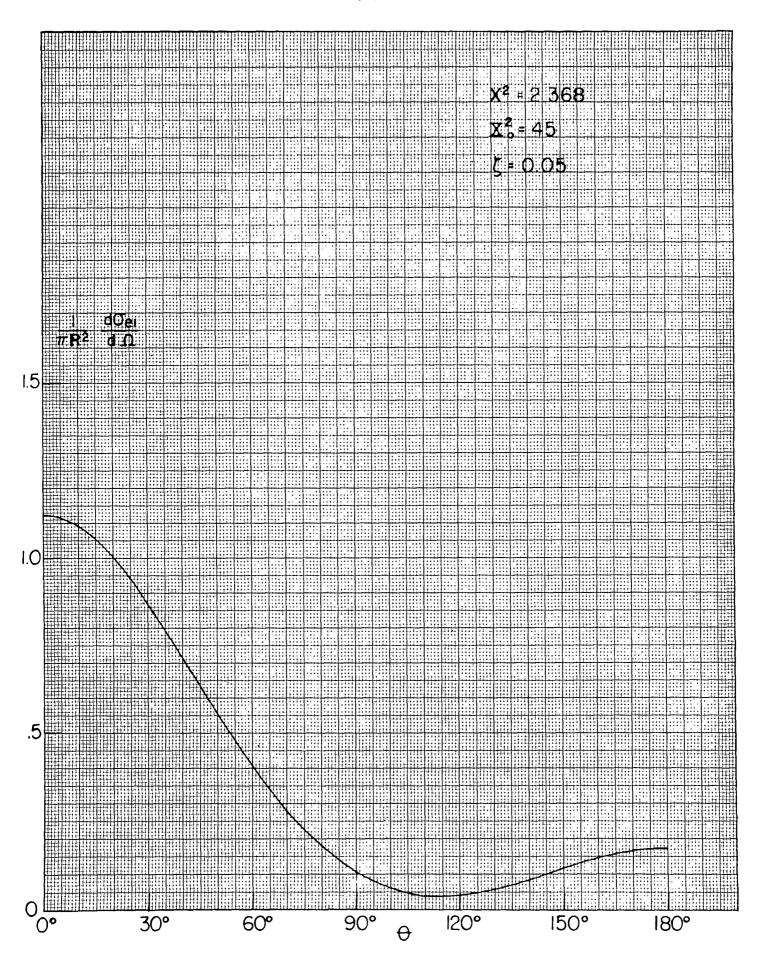
I X



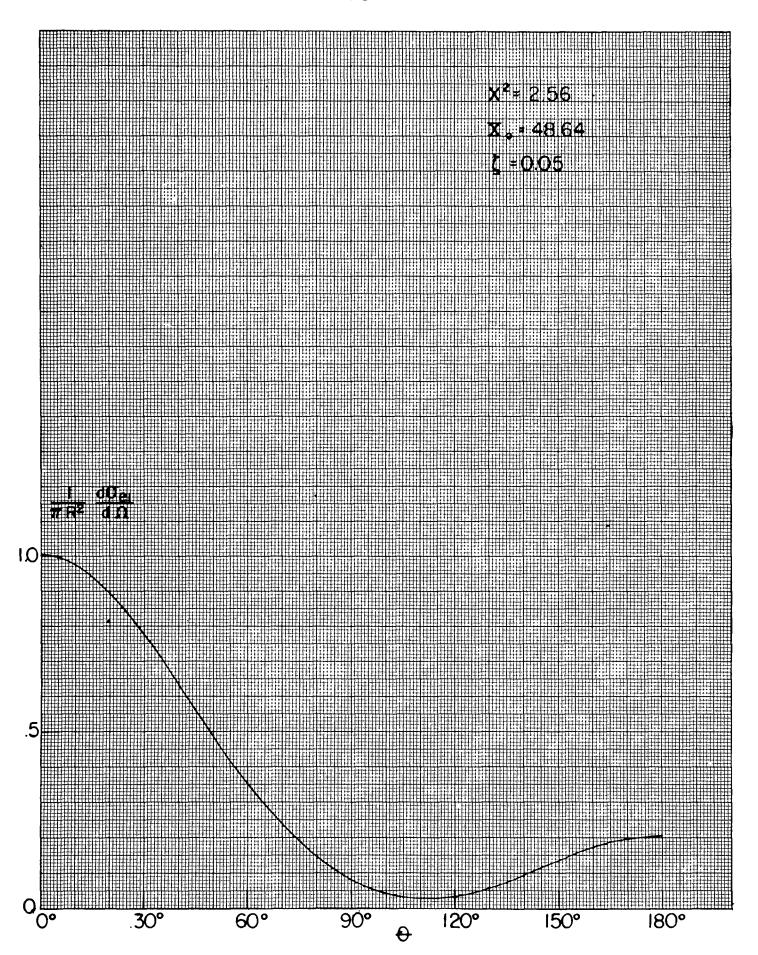


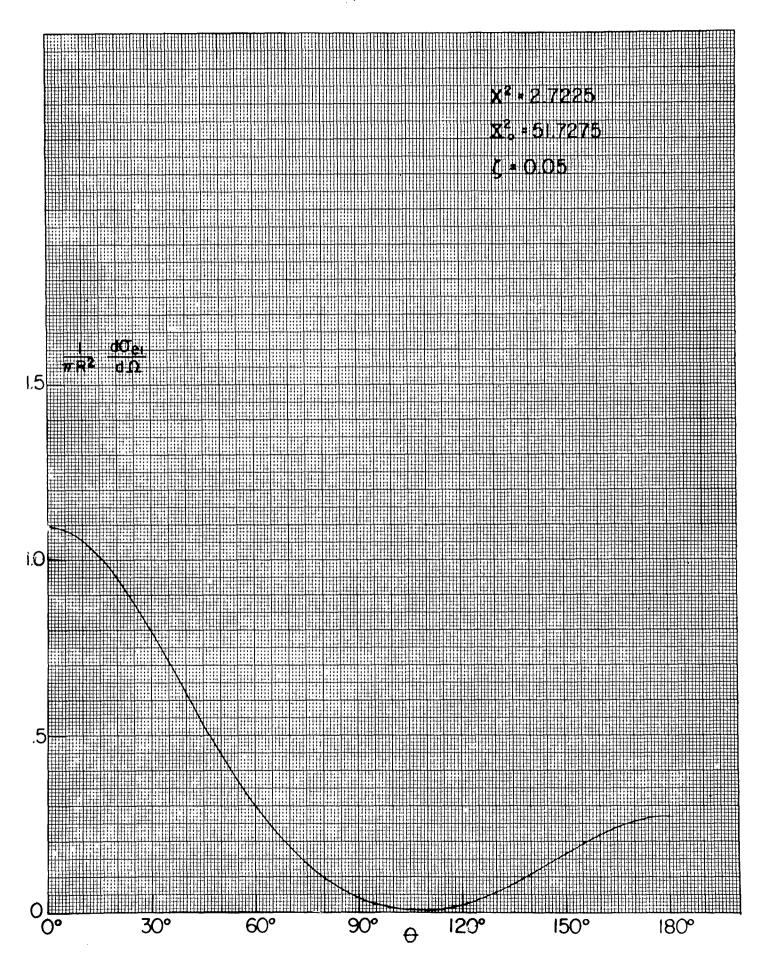


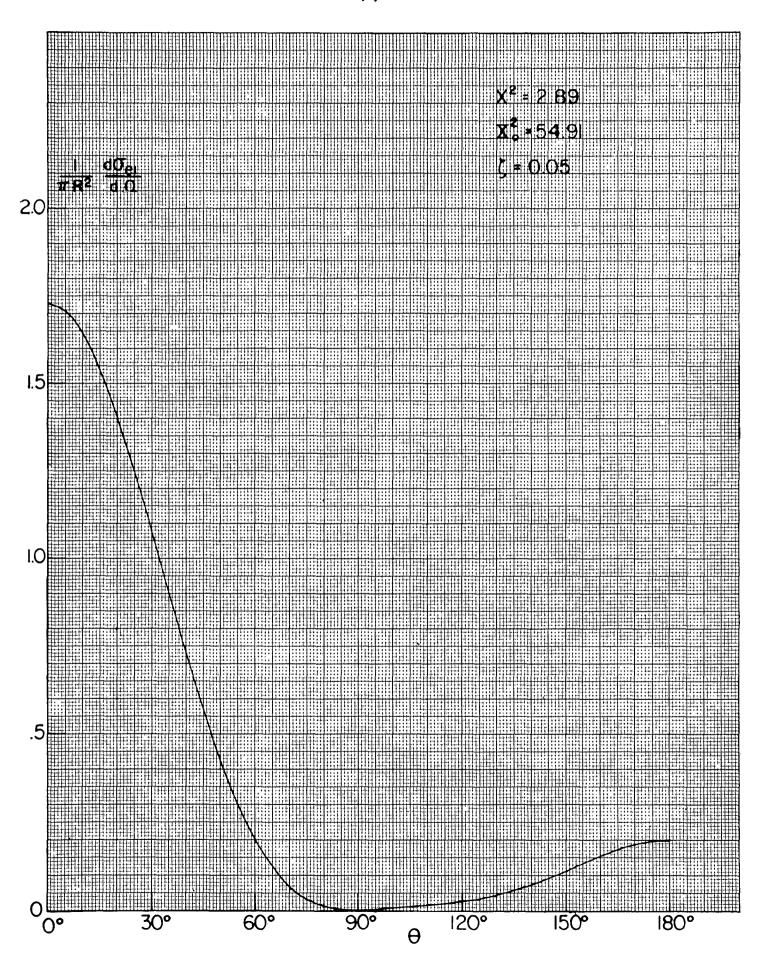


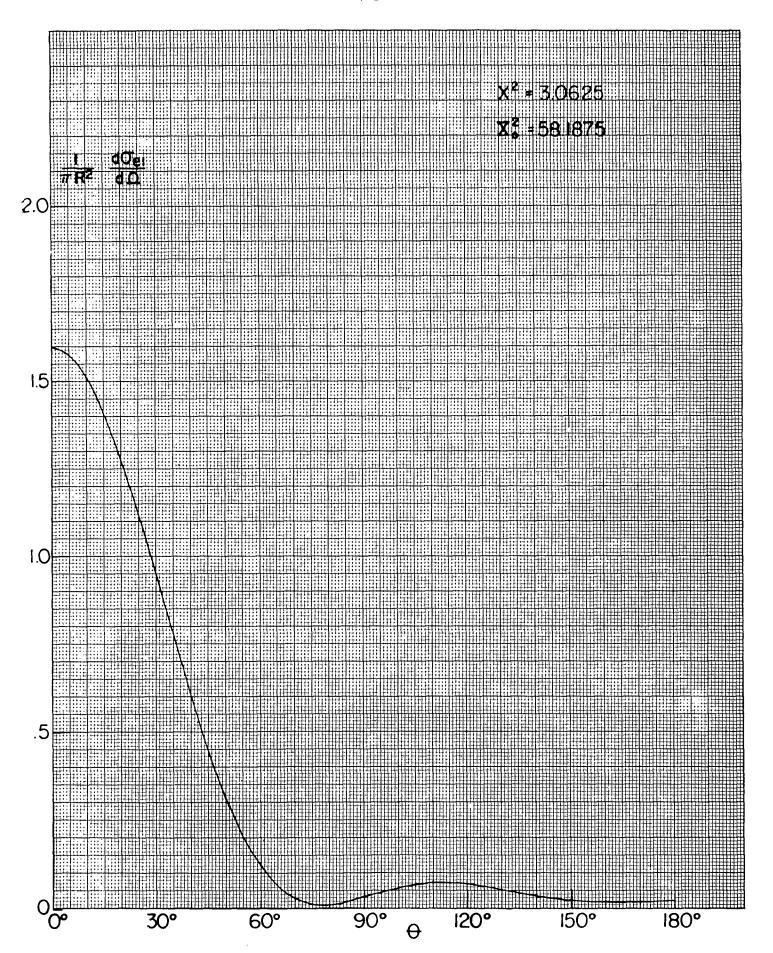


R. Am

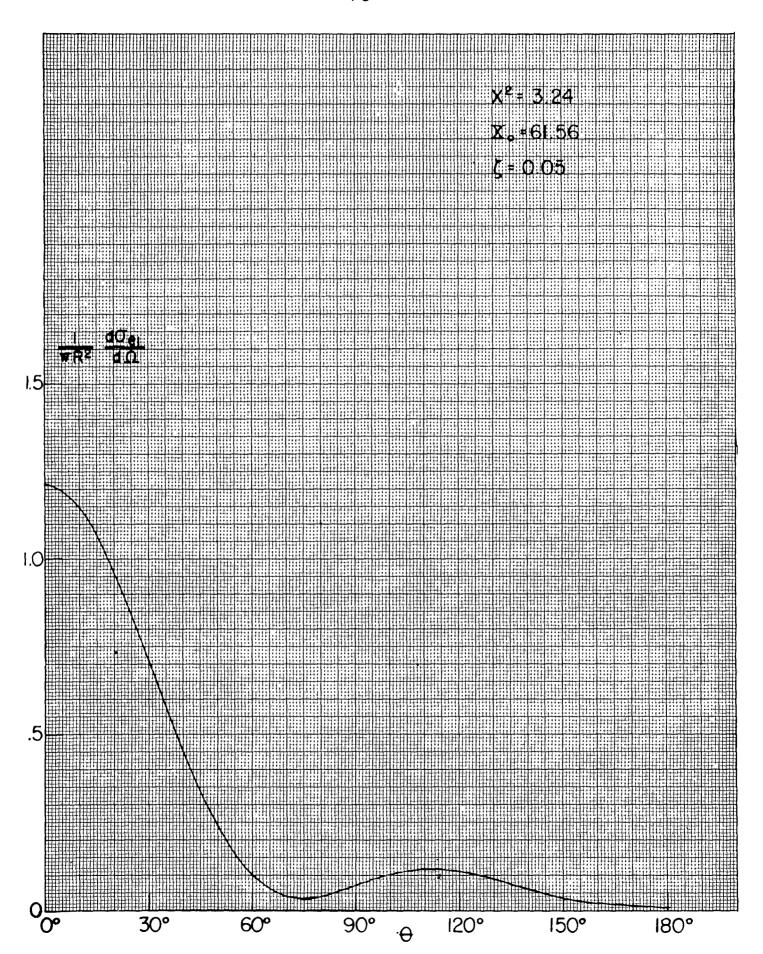


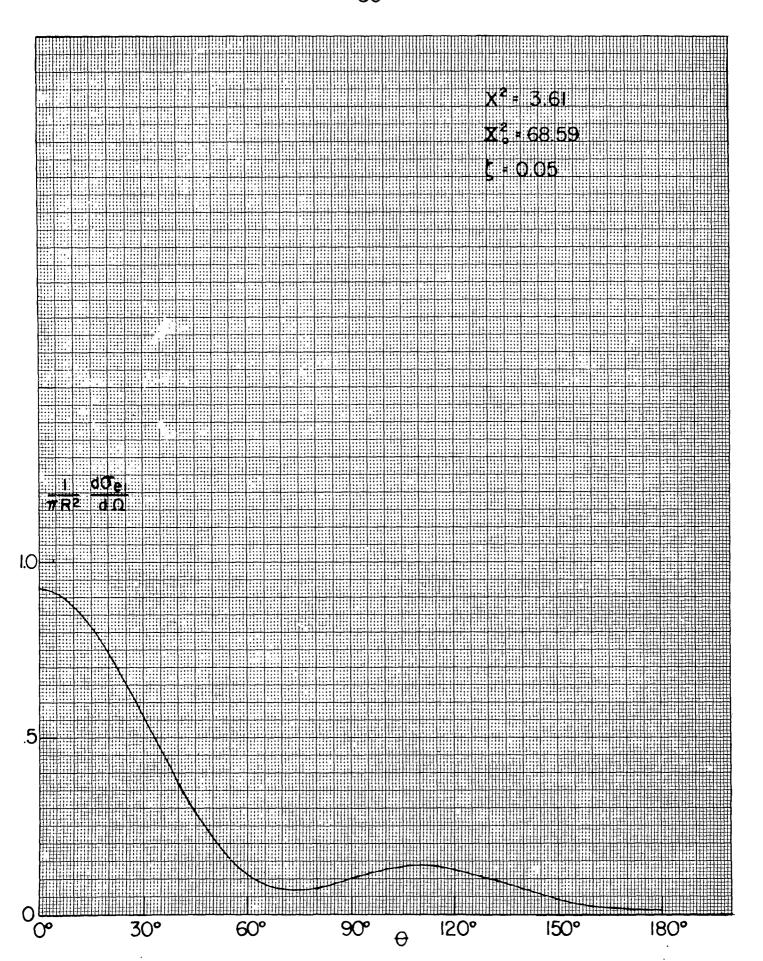


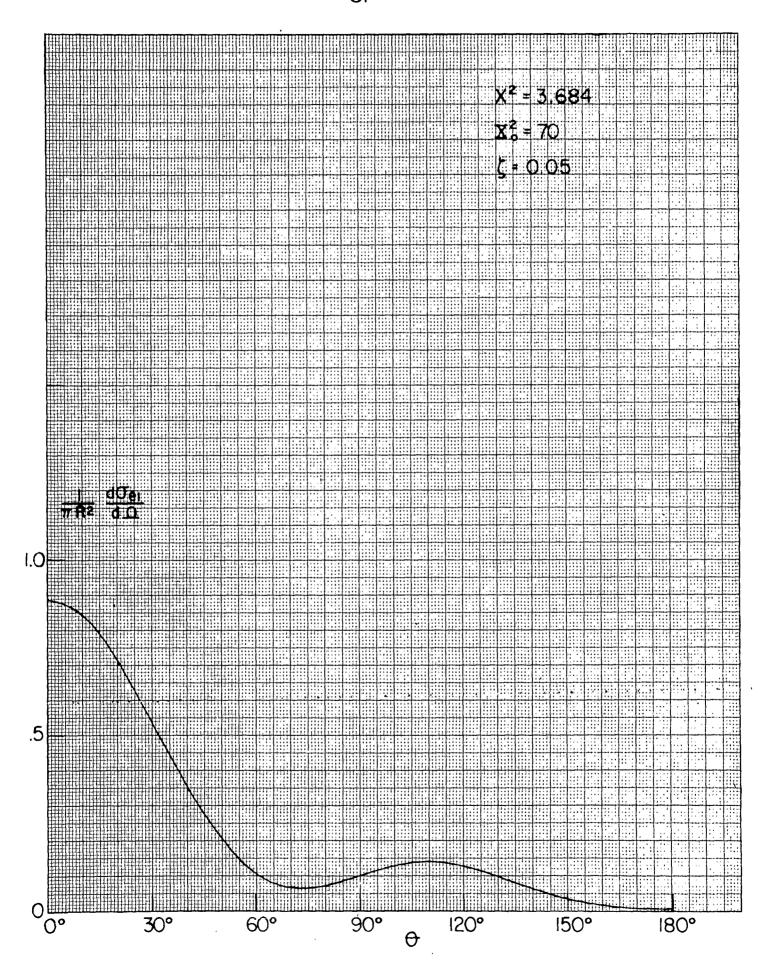


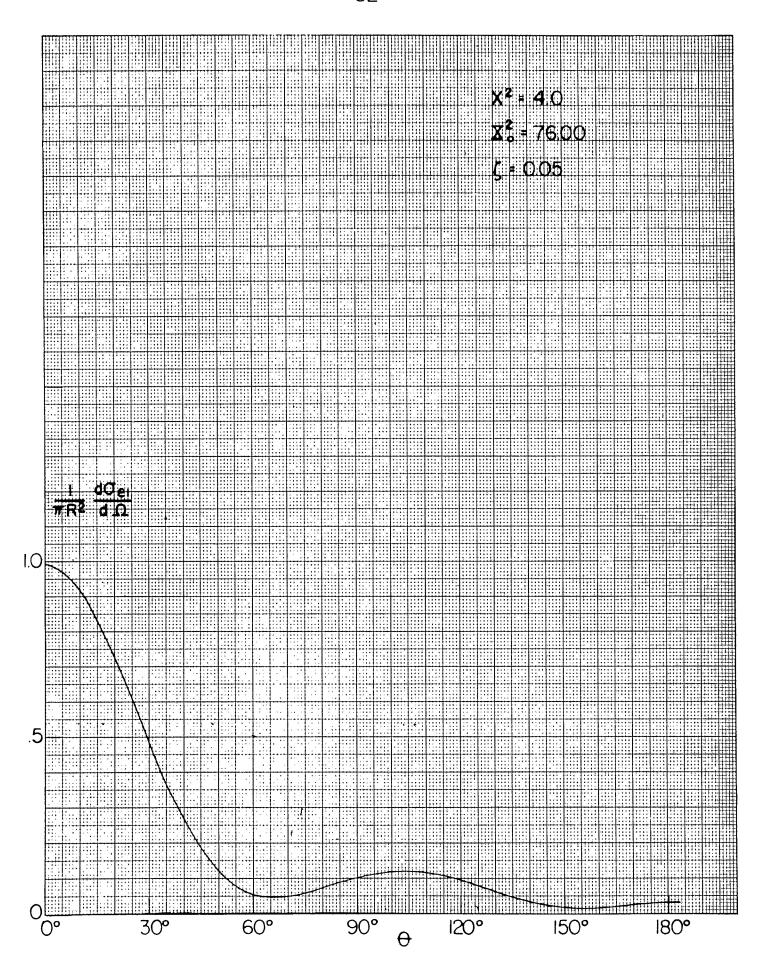


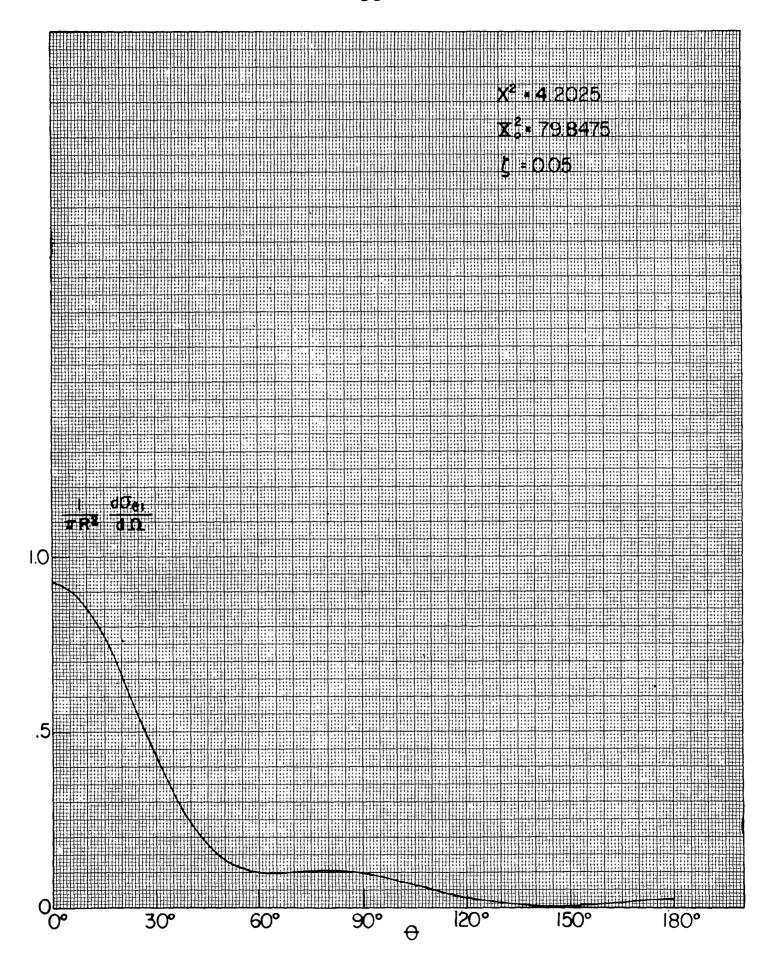
I I

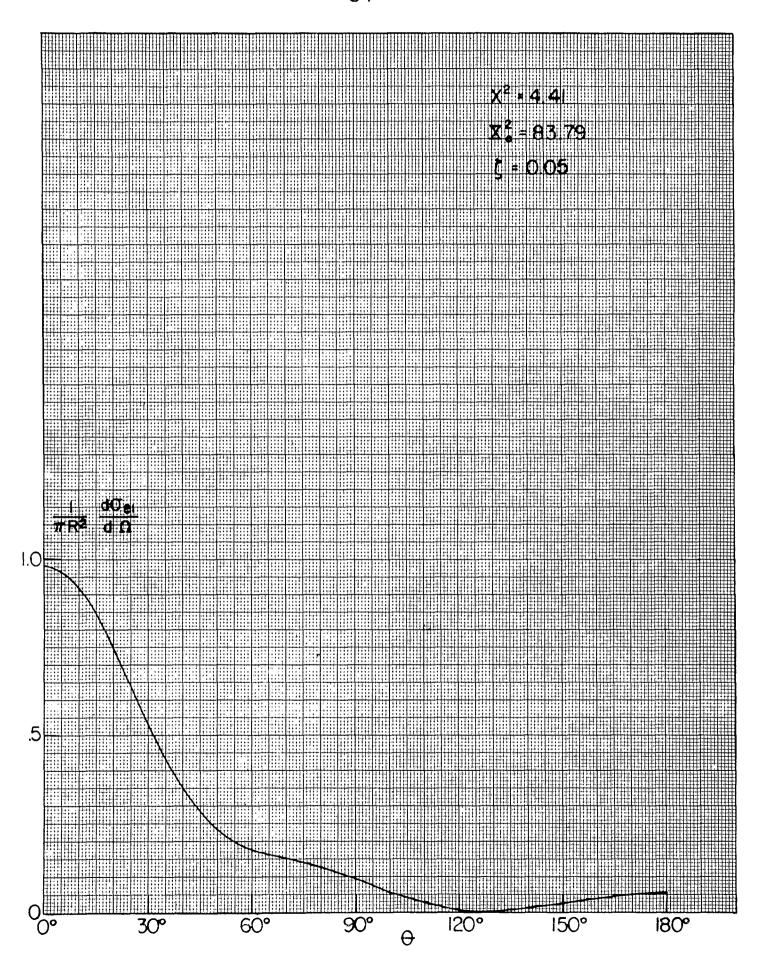




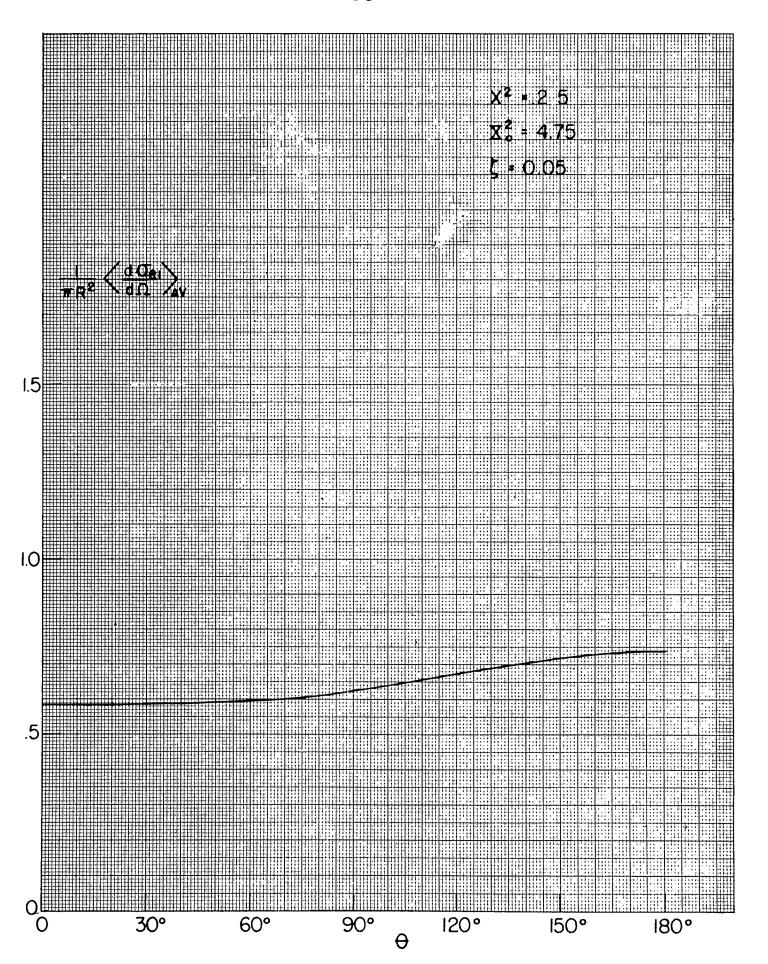


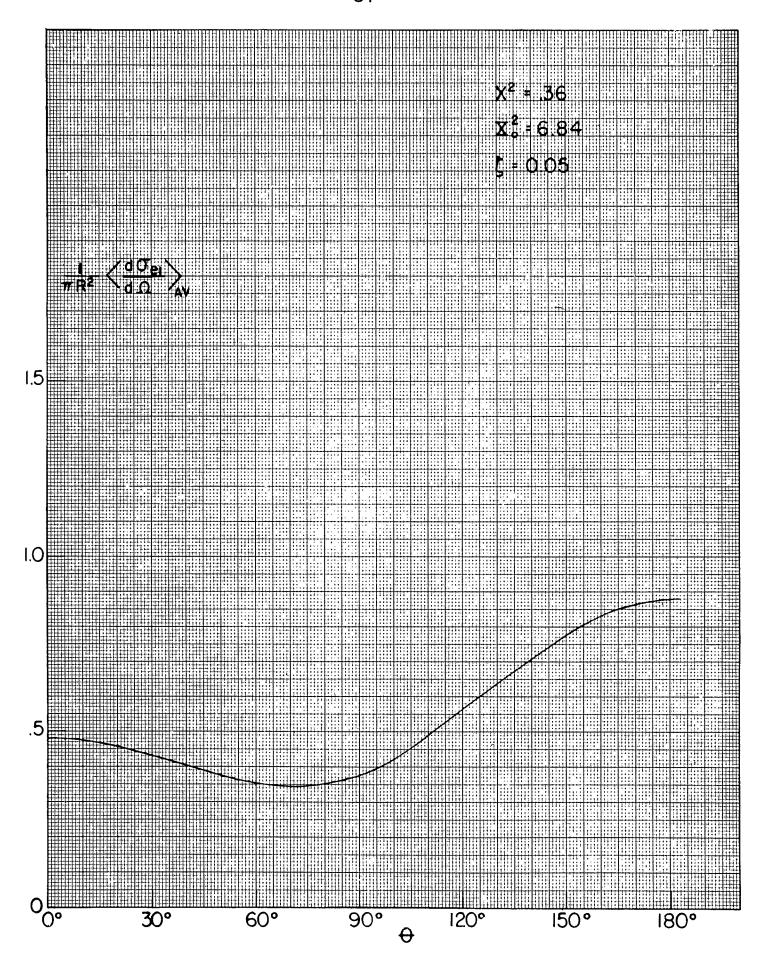


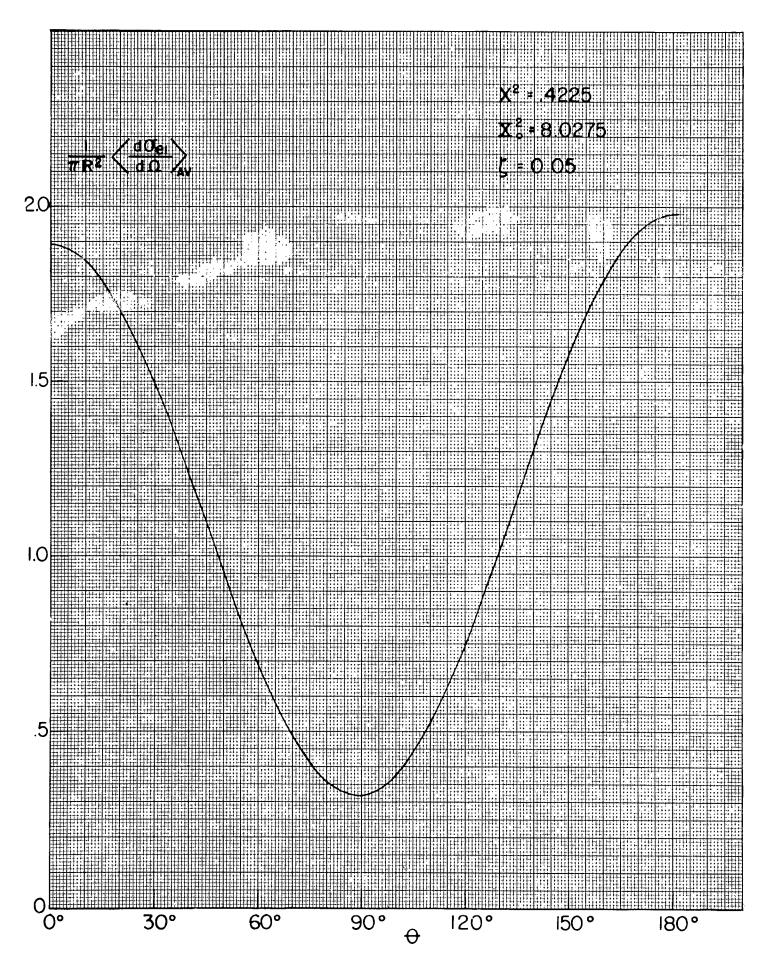


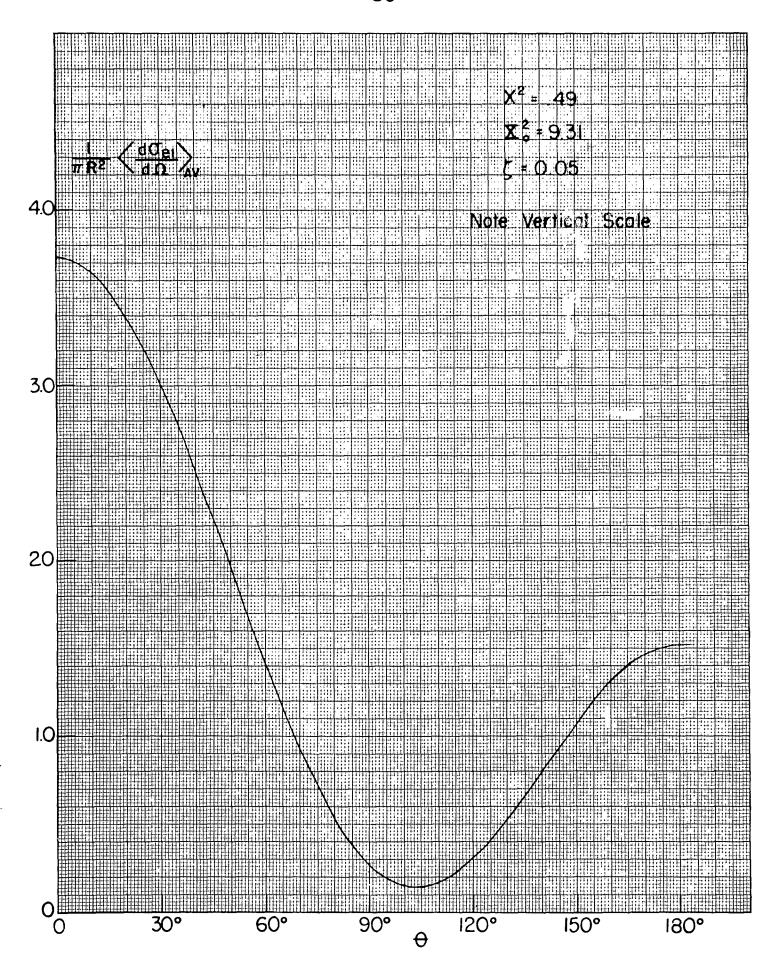


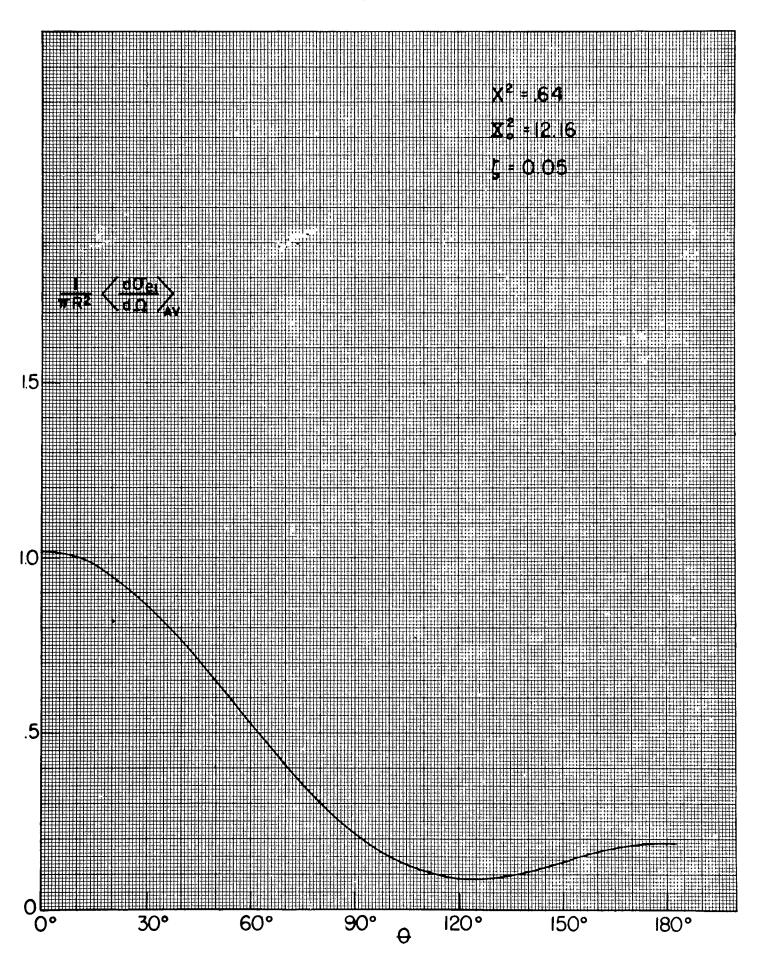
V. PLOTS OF DIFFERENTIAL CROSS SECTION FOR ELASTIC SCATTERING (SHAPE-ELASTIC + COMPOUND ELASTIC) FOR  $x^2/x_0^2 = 1/19$  WITH  $\zeta = 0.05$ 

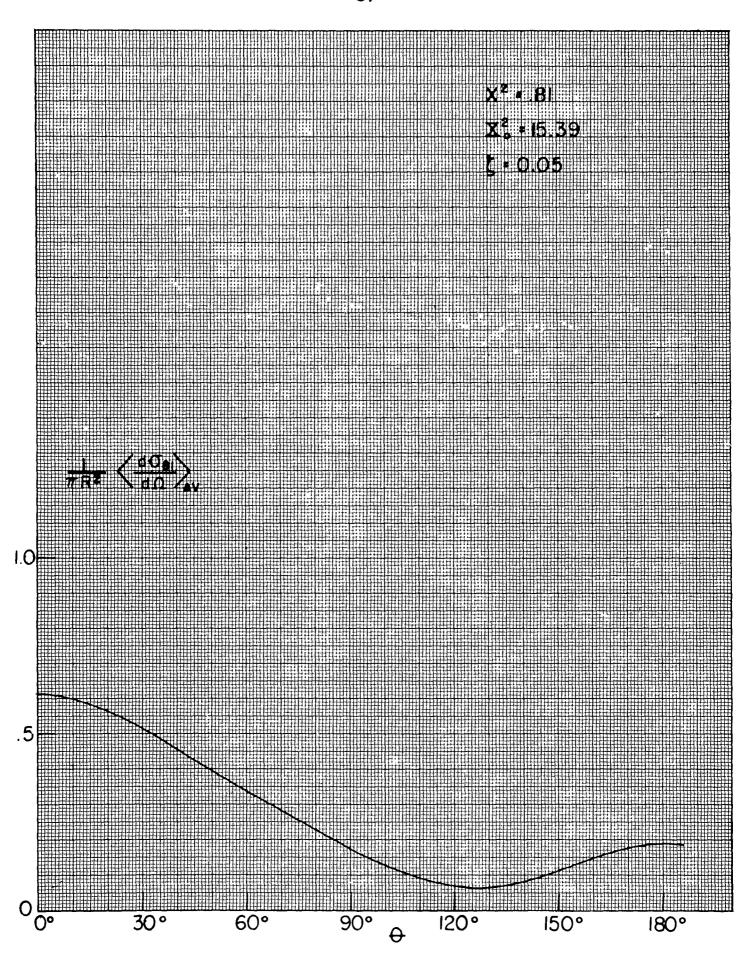


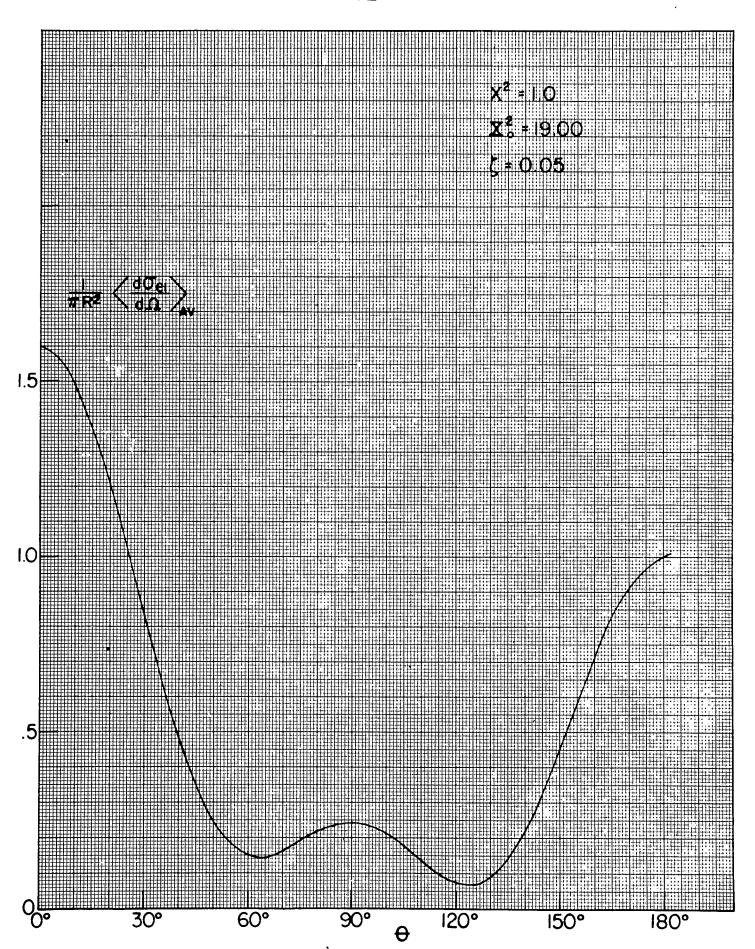


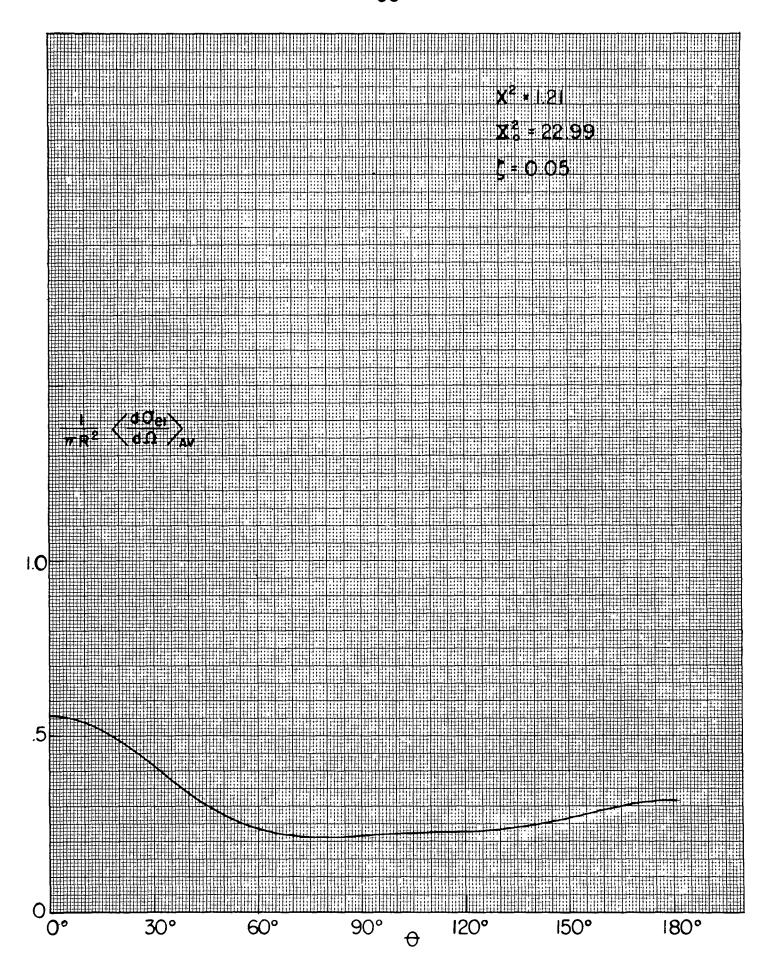


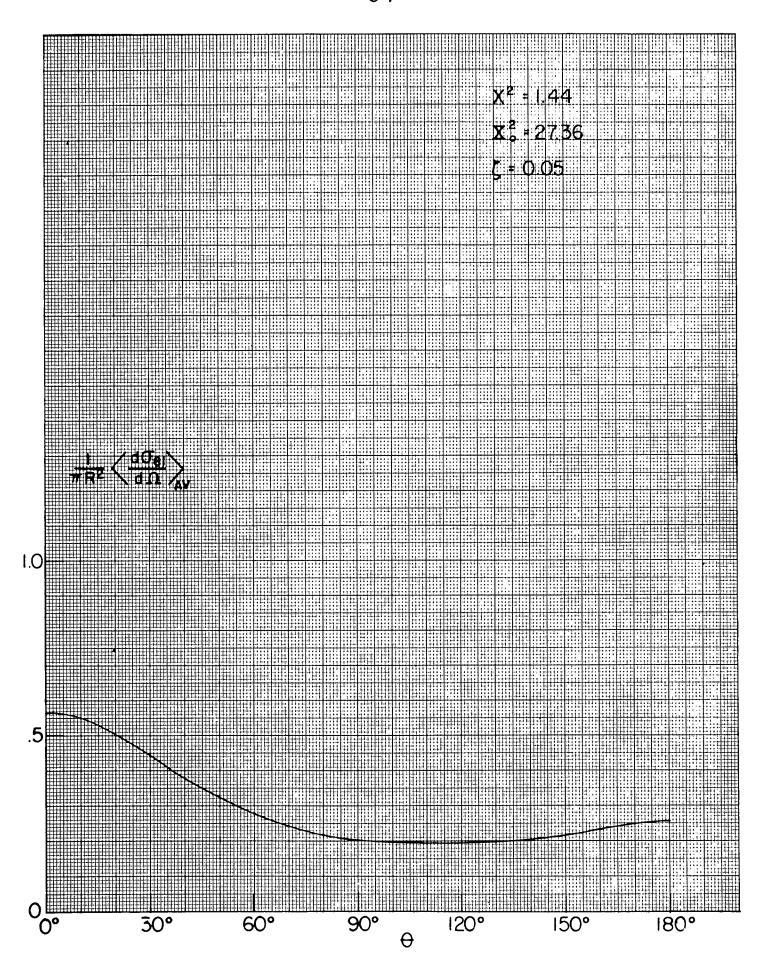


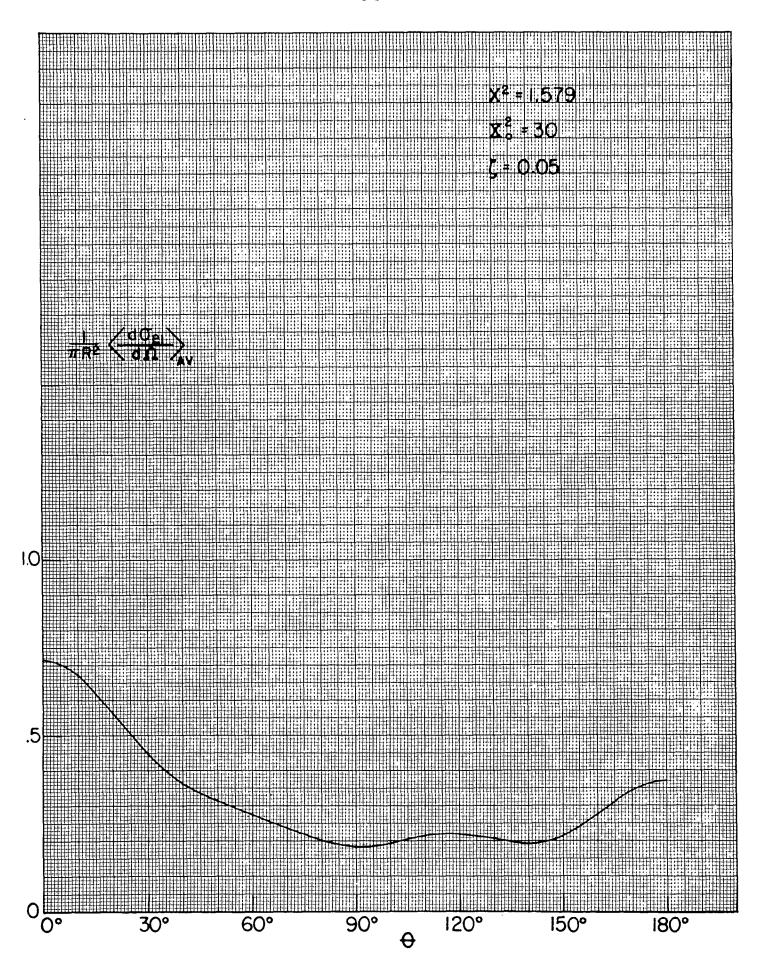


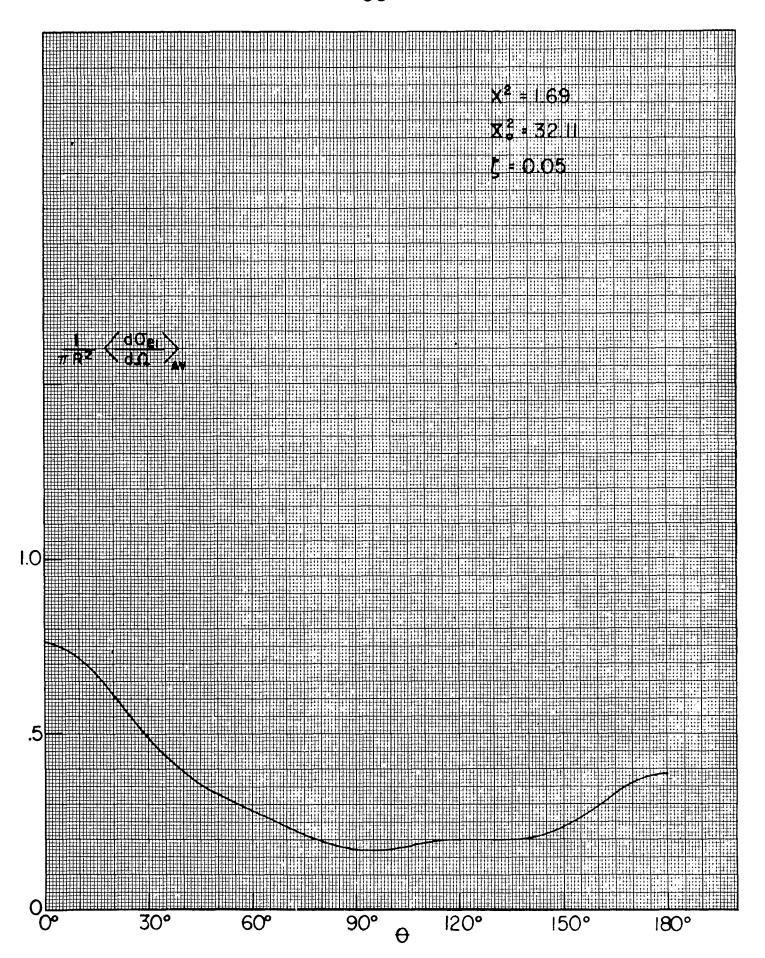


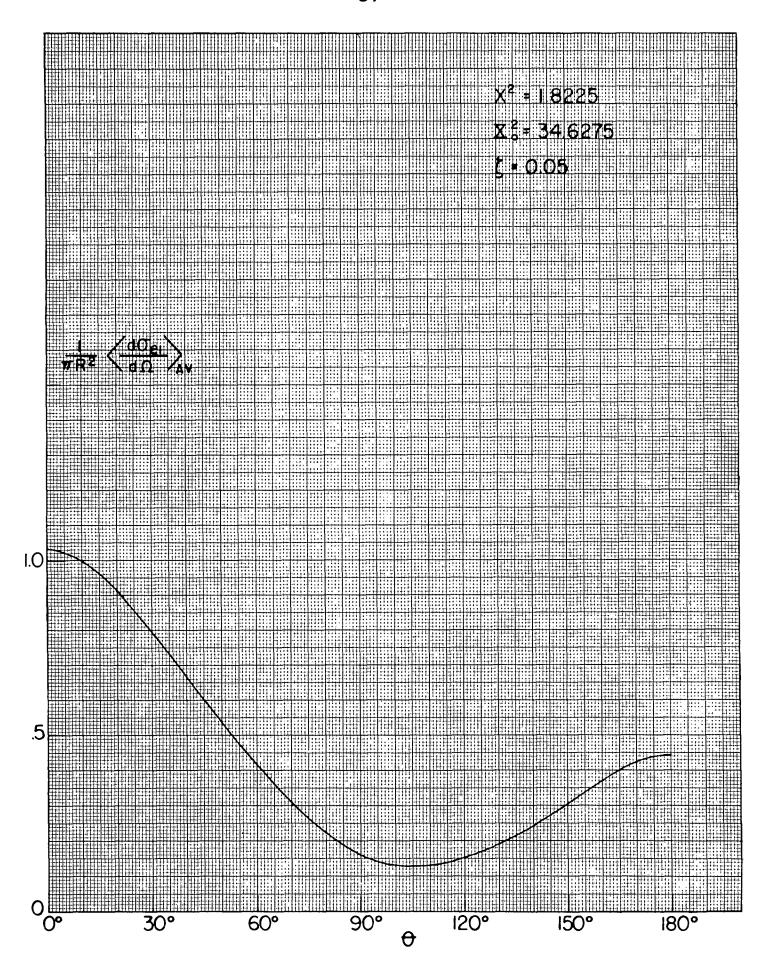


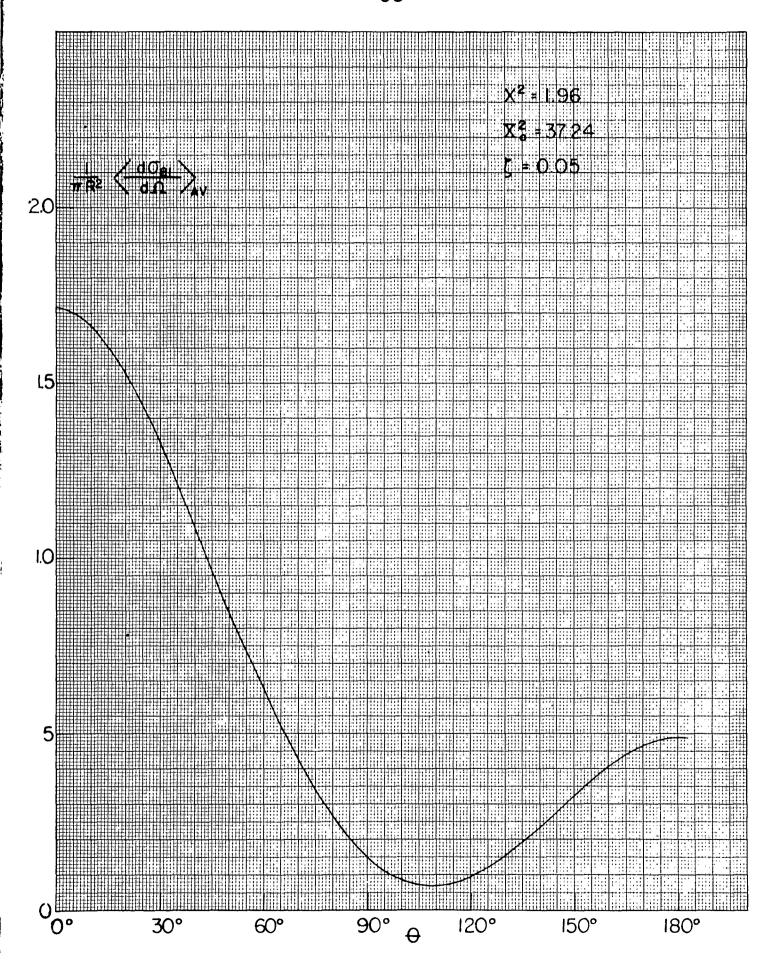


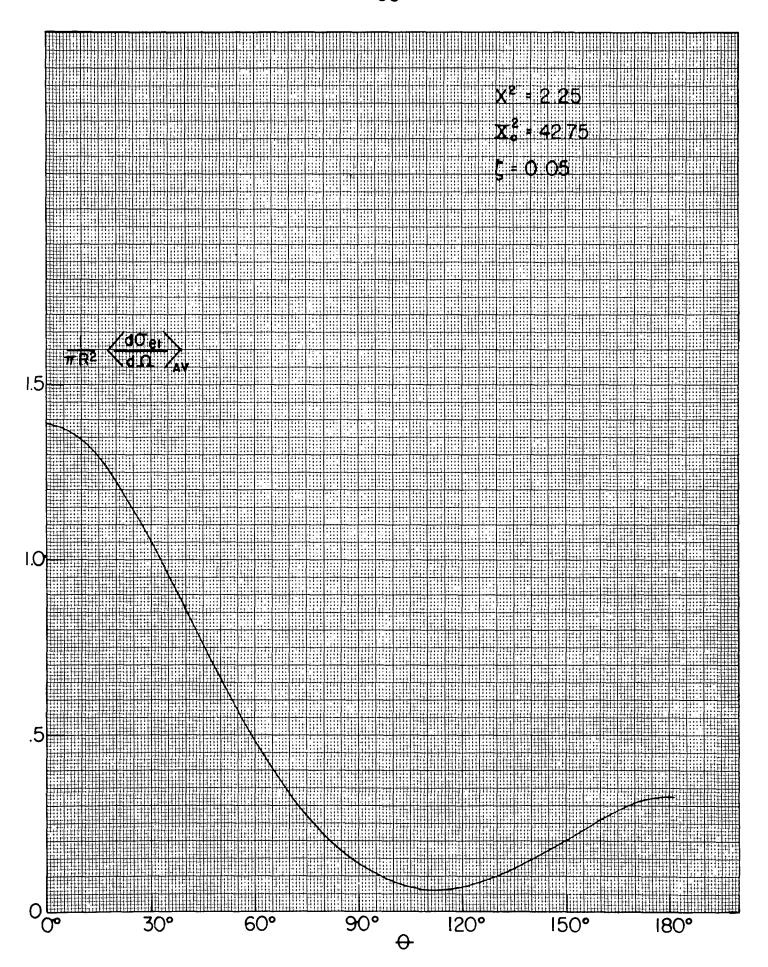


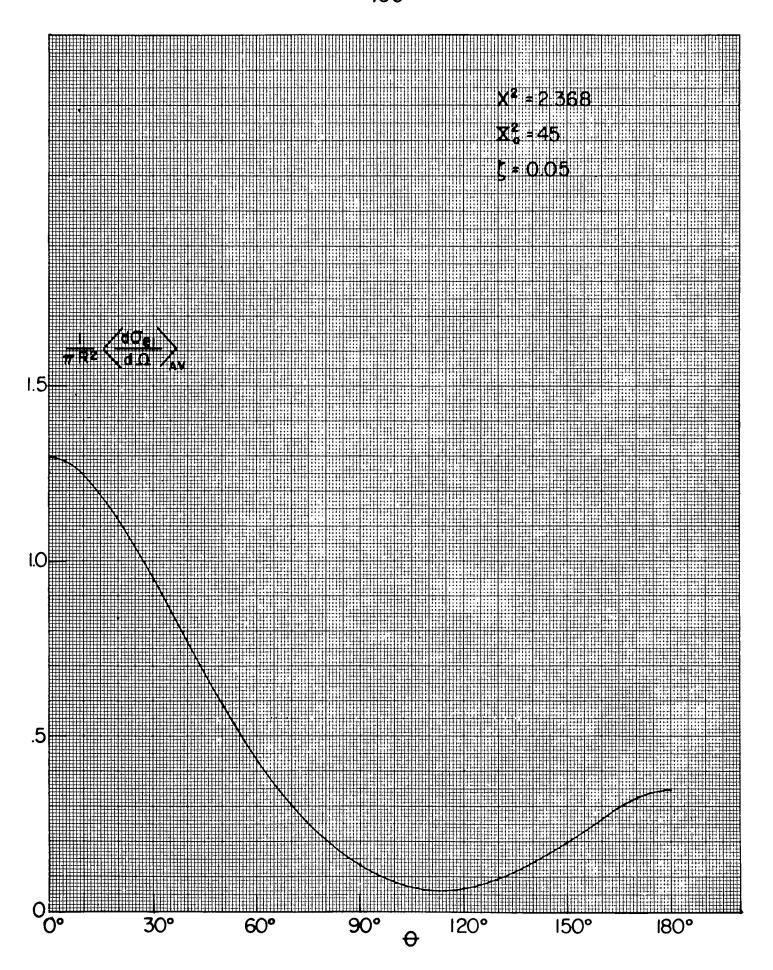


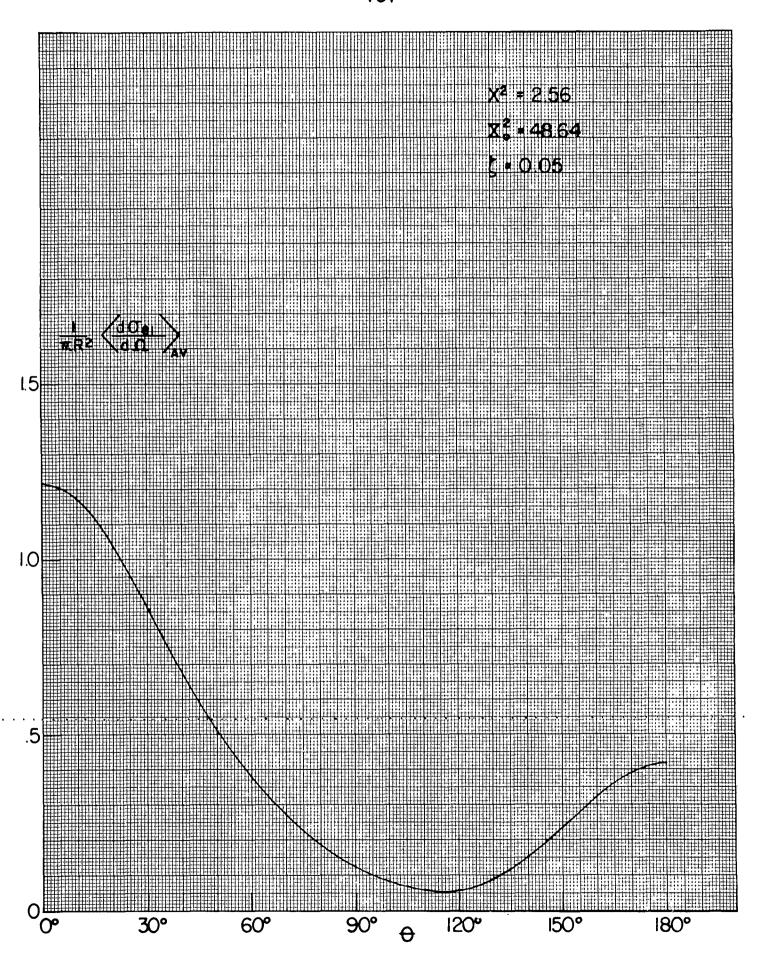


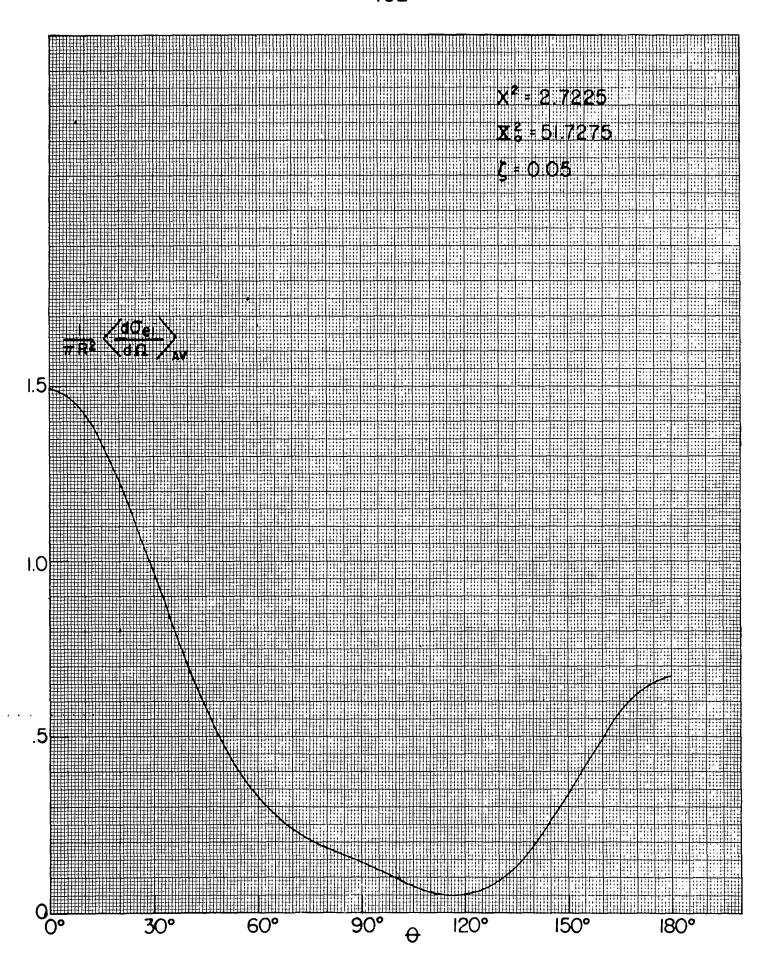


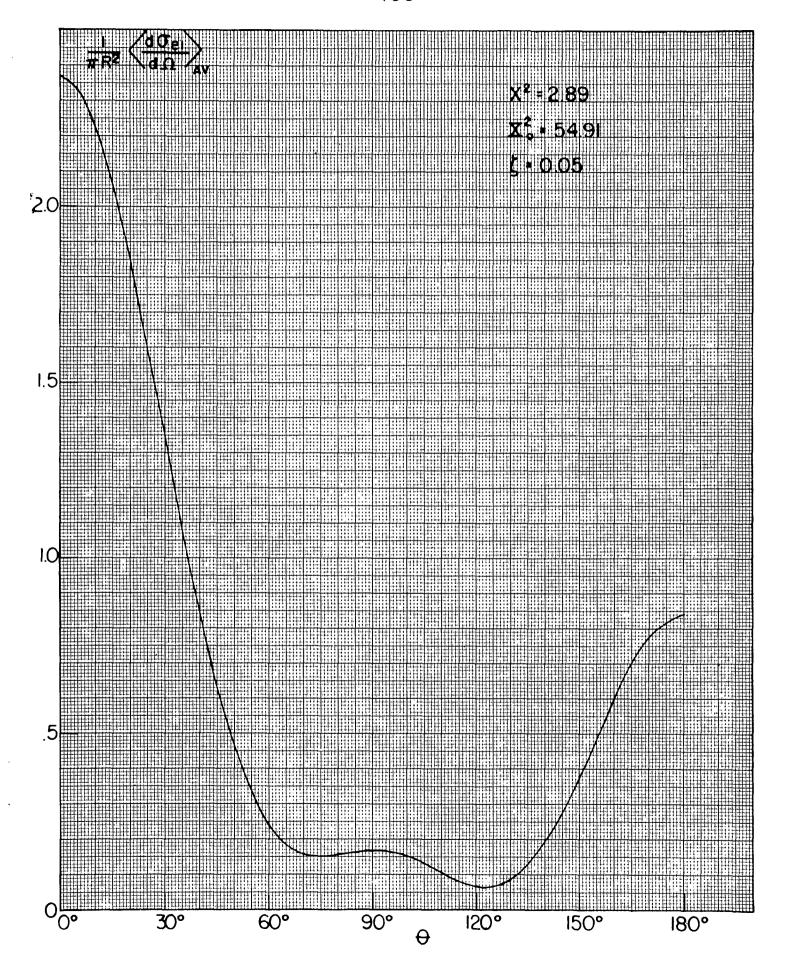


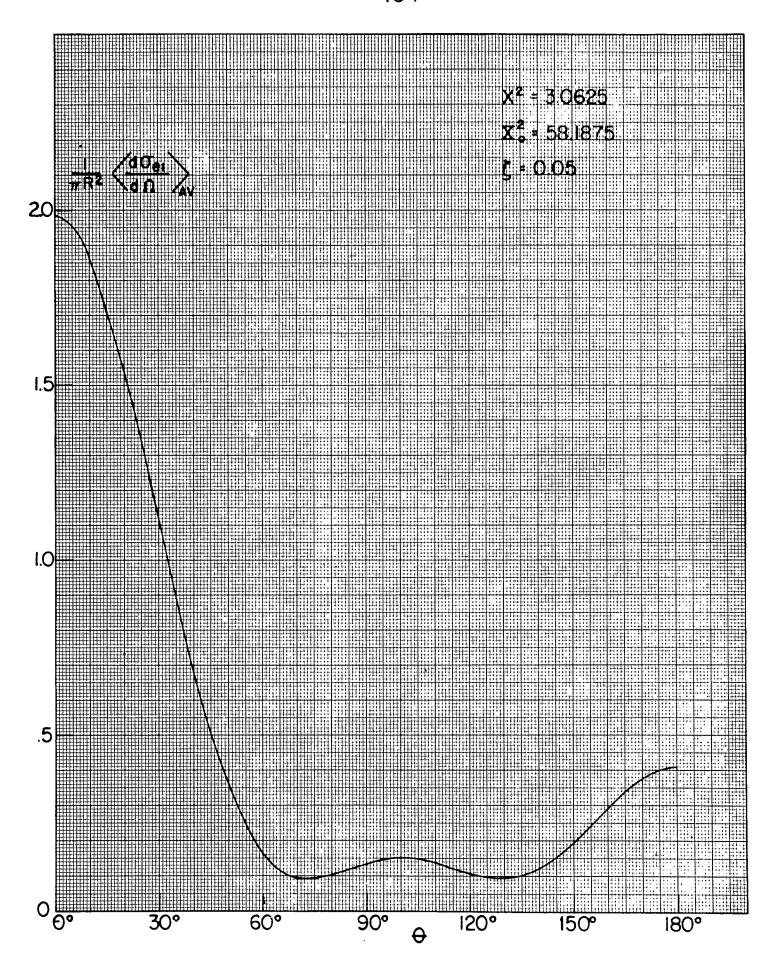


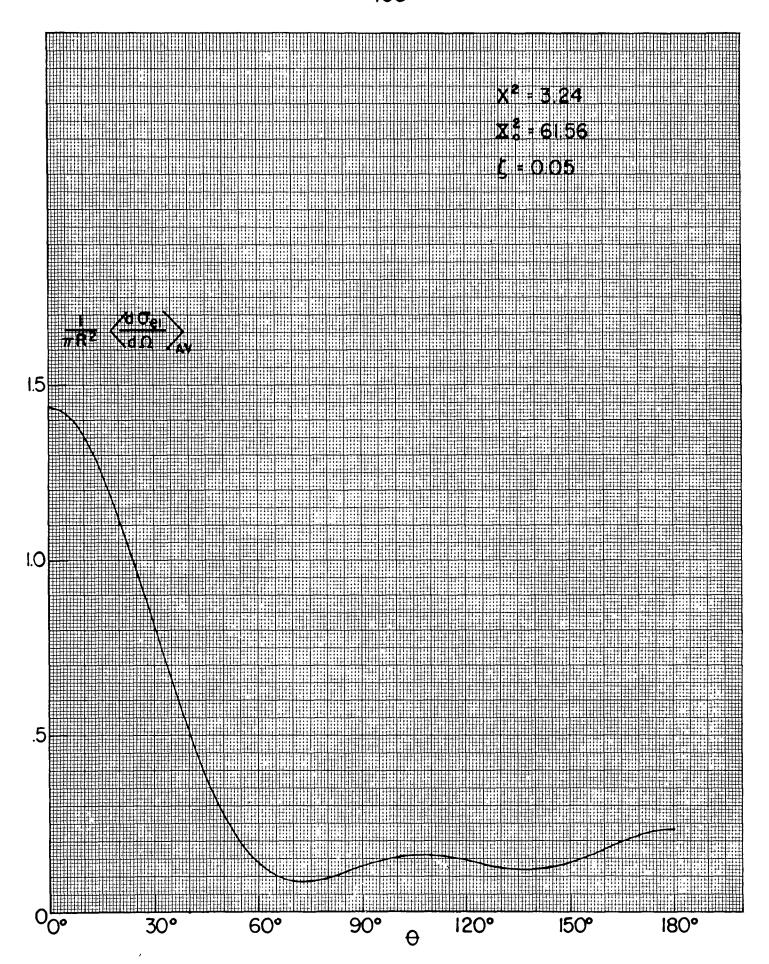


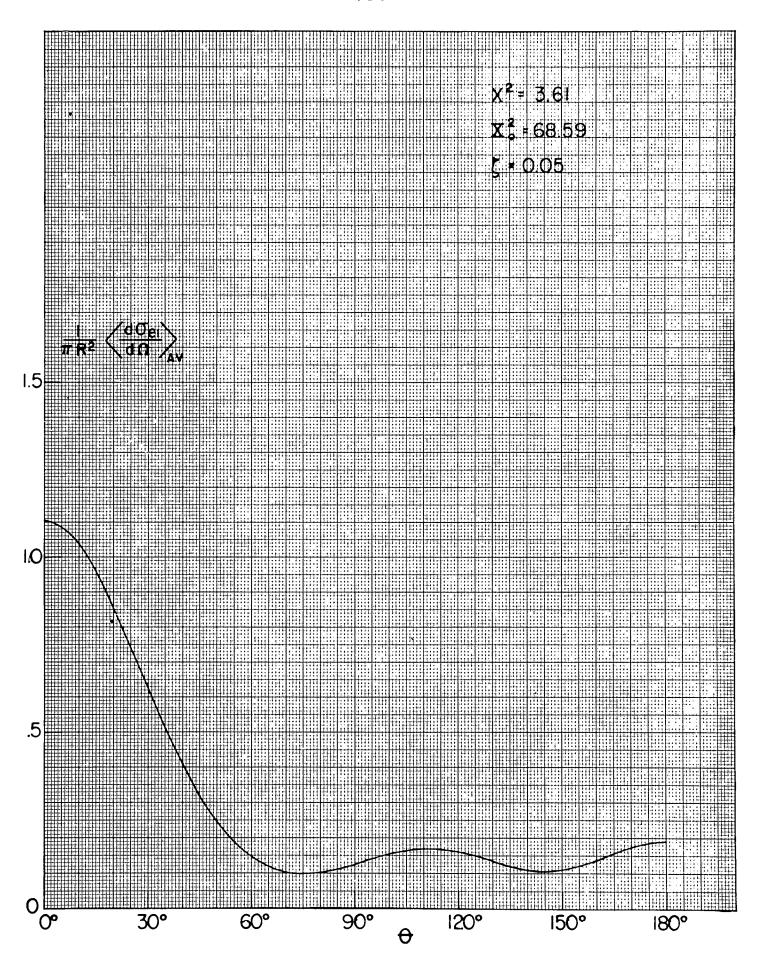


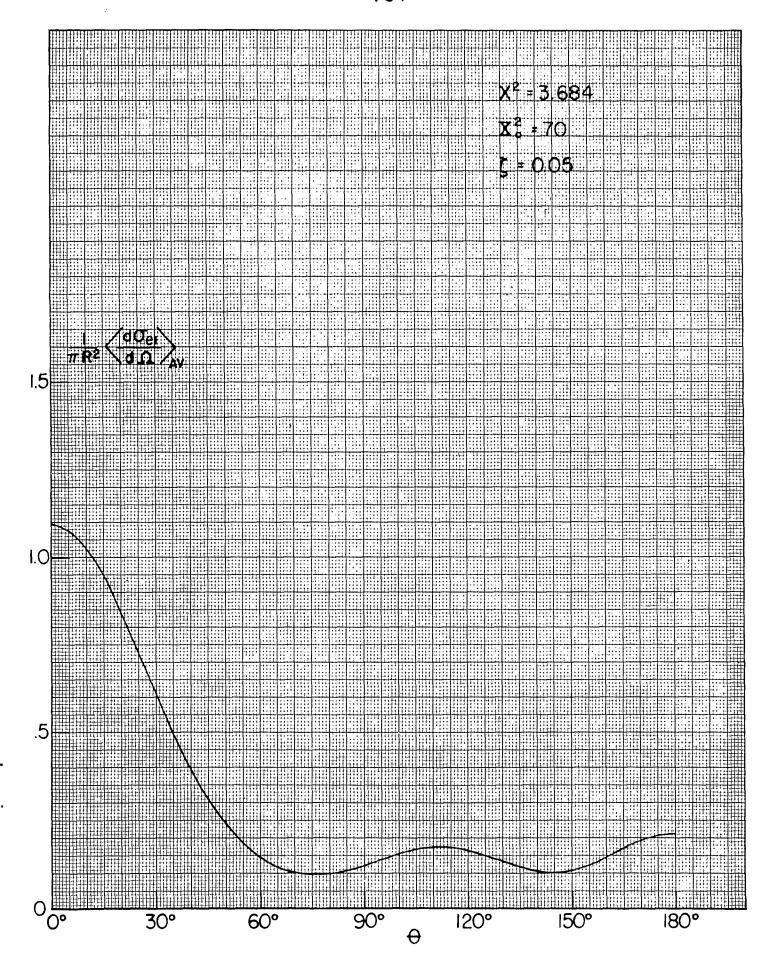


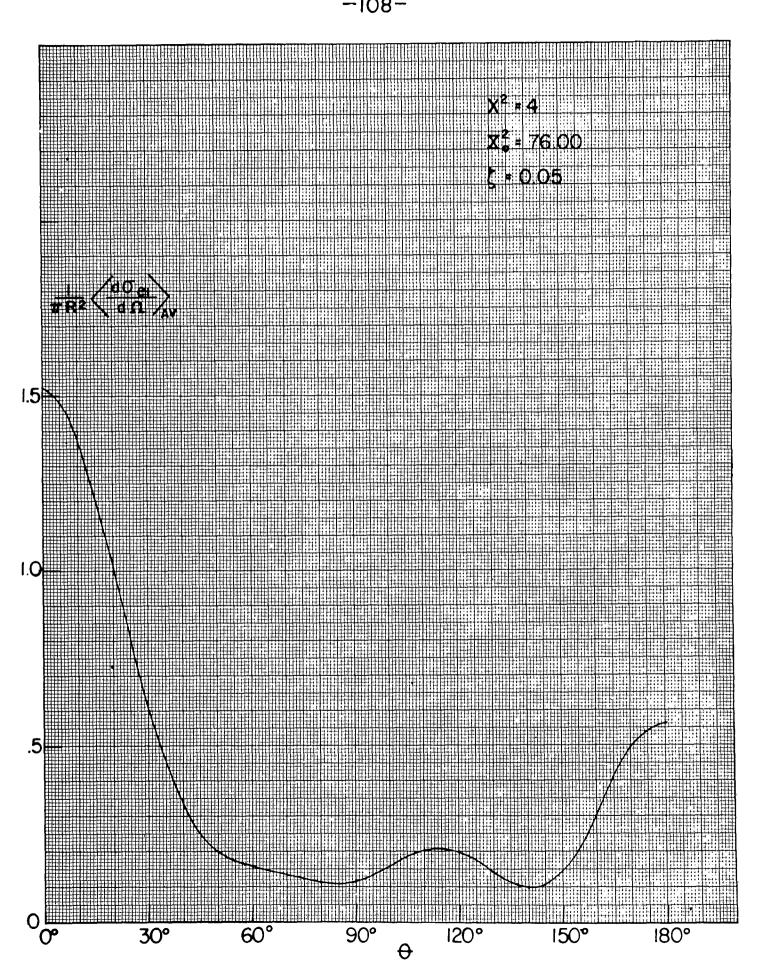


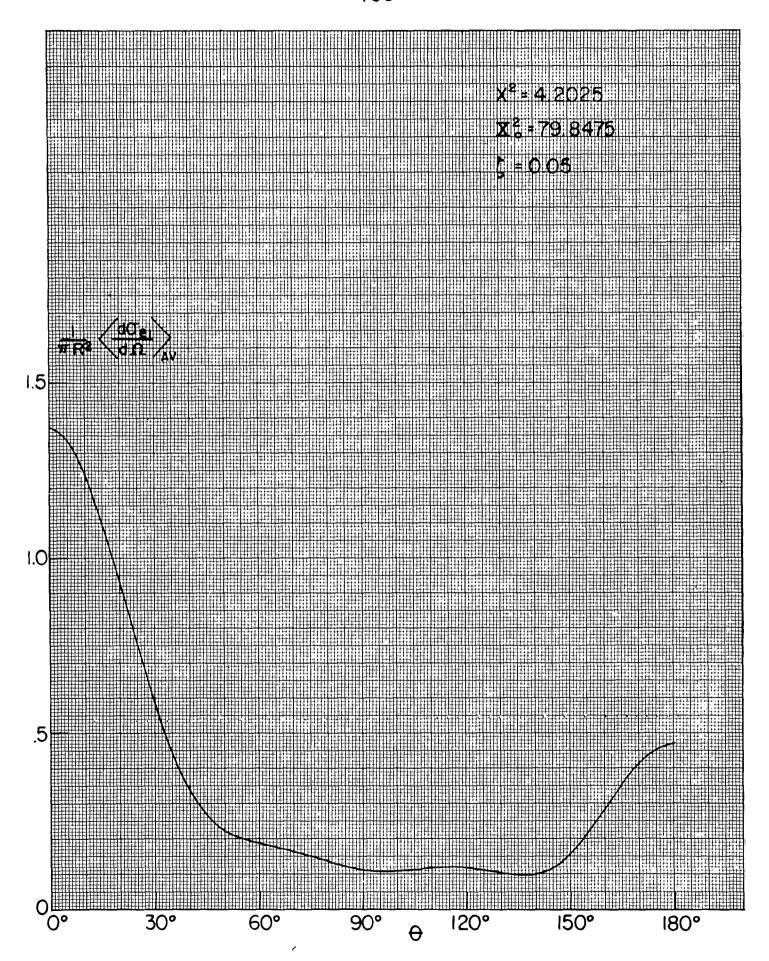


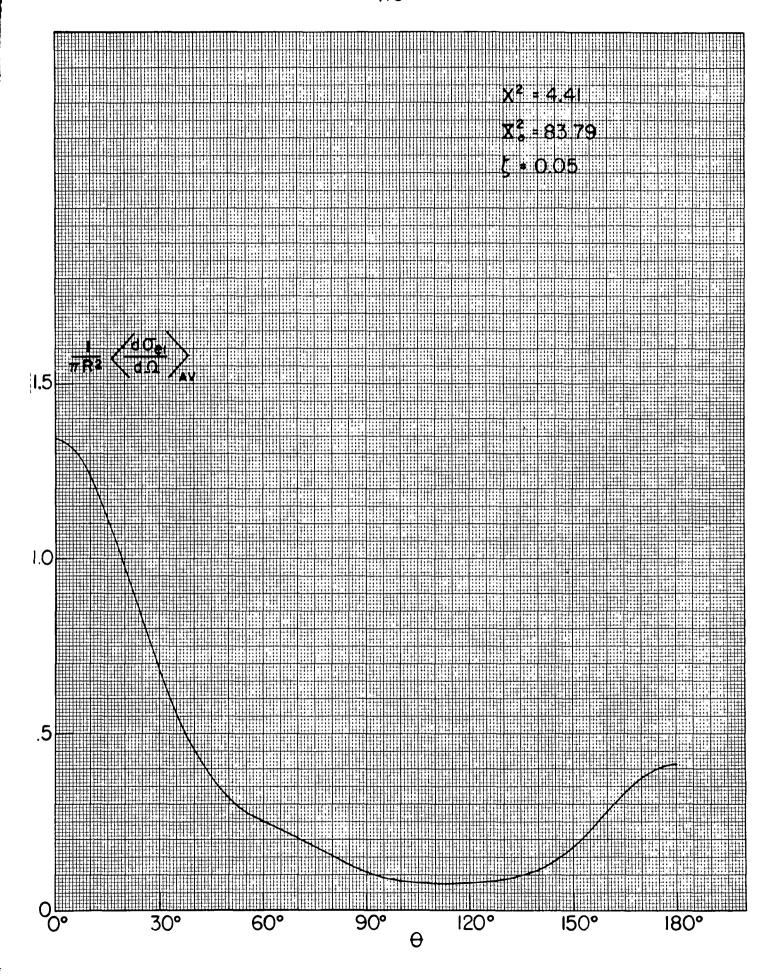












VI. TABLES OF  $s_{g}$ ,  $\Delta_{g}$ ,  $\cos 2 S_{g}$ ,  $\sin 2 S_{g}$ , AND  $\sin^{2} S_{g}$  FOR x = 0.1(0.1)3.0AND Q = 0(1)7

### *L* = 0

<u> </u>	_8_		<u>cos2</u> €	ein26	ein <sup>2</sup>
.1	= X	= 0	.98007	.19867	.0099667
:5			. 92106	.38942	.039470
.3			. 825 34	•56464	.087332
.4			-69671	.71736	.15165
•5			.54030	. 84147	.22984
•6			.36236	. 93204	.31882
.7			.16997	. 98545	.41502
.5			<b></b> 029 <i>2</i> 00	-99957	.51460
•9			22720	.97385	.61360
1.0			41615	. 90930	. 70807
1.1			58850	. 80850	.79425
1.2			<b></b> 73739	·67 <b>5</b> 46	. 86870
1.3			<b>8</b> 56 <b>89</b>	.51550	· 358/1
1.4			94222	. 33499	.97111
1.5			9899 <del>9</del>	.141120	. 99500
1.6			99829	058374	.99915
1.7			<b></b> 966 <b>50</b>	<b></b> 25554	. 98340
1.5			89676	44255	.94838
1.9			79097	61186	. 89548
2.0			6536 <sup>4</sup>	75680	. 82682
2.1			49026	87158	. <i>7</i> 4513
2.2			30733	<b>-</b> .95160	•65367
2.3			112153	<b></b> 99369	.55608
2.4			.087499	99616	.456 <b>25</b>
2.5			• 28366	95892	.35817
5.6			.46852	88345	.28366
2.7			·63 <sup>1</sup> 69	77276	.18265
2.8			.77557	63127	.112217
2.9			.88552	46460	.057240
3.0			.96017	27942	.019915

#### *L* = 1

*	8		<u>cos?</u> 6	sin?6	sin <sup>2</sup>
.1	.0009901	99010	1.000000	.000663	.1098 (-6)
.2	.007692	<b>-</b> .96154	. 99999	.005209	6.7831 (-6)
•3	.024771	91743	. 99985	.017086	.072985 (-3)
•#	.055172	86207	. 99924	.038977	.37995 (-3)
•5	.100000	80000	•99736	.072641	1.32091 (-3)
•6	.15882	73529	. 99291	.118879	3.5456 (-3)
.7	.23020	67114	.98410	.17760	7.9487 (-3)
.8	.31219	60976	.96878	.24790	.015608
•9	.40277	55249	.94462	.32817	.027691
1.0	.50000	50000	.90930	.41615	.045351
1.1	.60556	45249	. 86076	.50901	.069621
1.2	. 70820	40983	<b>. 7973</b> 6	.60350	.101319
1.3	.81673	37175	.71805	69599	.1409 <b>75</b>
1.4	.92702	33784	.62247	. 78265	.18877
1.5	1.03846	30769	.51100	. 85958	. 24450
1.6	1.150 <b>5</b> 6	28090	.38498	.92292	. 30751
1.7	1.26298	25707	.24638	.96917	.37681
1.8	1.37547	<b></b> 23585	.098034	.99518	.45098
1.9	1.48785	21692	<b>0</b> 56767	.99839	.52838
5.0	1.6000	20000	21326	.97700	.60663
2.1	1.7118	18484	36762	92998	.68381
2.2	1.8233	17123	51488	. 85726	. 75744
2.3	1.9343	15898	65021	·75975	. 82511
2.4	2.0450	14793	76895	.63931	. हहभभ्
2.5	2.1552	13793	86674	.49876	•93337
5.6	2.264 <b>9</b>	12887	93977	.34181	• 96989
2.7	2.3743	12063	98494	.17290	.99247
2.8	2.4833	11312	999996	002863	•999 <del>99</del> 8
2.9	2.5918	10627	98368	17995	.99184
3.0	2.7000	10000	93579	35257	•96789

1 = 2

	_\$_		cos 26	<u>ein 26</u>	ein 25
.1	1.10741 (-6)	-1.9%7	1.000000	.000000	.000000
.2	.035082(-3)	-1.9865	1.000000	.000014	.000000
.3	.26191 (-3)	-1.9692	1.000000	.000106	.0028 (-6)
.4	1.07726 (-3)	-1.9 <del>44</del> 1	1,000000	.000438	.0479 (-6)
.5	3.1847 (-3)	-1.9108	•999999	.001307	.4268 (-6)
•6	7.6164 (-3)	-1.5688	• <b>99</b> 9995	.003162	2.4999 (-6)
.7	.015693	-1.8179	.999978	.006611	.0109266(-3)
.8	.028922	-1.7582	•999923	.012397	.038423 (-3)
.9	.048857	-1.6904	• <b>99</b> 9772	.021364	.114123 (-3)
1.0	.076923	-1.6154	.99 <del>9\</del> 08	<b>.03</b> 4406	.29603 (-3)
1.1	.114269	-1.5347	.99863	<b>.0</b> 52400	.68691 (-3)
1.2	.16165	-1.4500	.99710	.076149	1.45178 (-3)
1.3	.21936	-1.3630	•9 <del>9</del> 433	.106319	2.8340 (-3)
1.4	.28727	-1.2756	·9 <b>8</b> 967	.143384	5.1665 (-3)
1.5	.36486	-1.1891	.98225	.18759	8.8760 (-3)
1.6	.45132	-1.1053	.97104	.23890	.0144775
1.7	.54564	-1.0249	.95488	.29699	.022560
1.5	·6 <del>4</del> 672	9487	.93248	.36122	.033760
1.9	.75348	8773	. 90253	<b>.</b> 43062	.048734
2.0	.86487	8108	.86376	.50390	.068120
2.1	•97991	7493	. 81501	.57944	.092494
2.2	1.09779	6928	<b>.</b> 75533	·6553 <sup>14</sup>	.122335
2.3	1.21776	6408	· Estot	.71665	.15798
5.4	1.33921	5933	.60080	.79940	.19960
2.5	1.46165	5392	.50571	.86270	.24715
2.6	1.5847	5106	. 39931	.91682	. 300 35
2.7	1.7079	4746	.28262	<b>•95</b> 923	•35869
2.5	1.8312	4416	.15719	.98757	.42140
2.9	1.9542	4119	.025032	•99969	.48748
3.0	2.0769	3846	111374	.99378	•55569

## **!** = 3

<u>*</u>	_8_	Δ	co = 26	ein 26	sin ?6
_	<b></b>				
.1	·44356 (-9)	-2.9980	1.000000	.000000	.000000
.2	.056435 (-6)	<b>-</b> 2.9920	1,000000	.000000	.000000
•3	.95460 (-6)	-2.9819	1.000000	.000000	000000
.4	7.0512 (-6)	-2.9676	1.000000	.000002	000000
•5	.033014 (-3)	-2.9491	1.000000	.000010	000000
•6	.115664 (-3)	-2.9260	1,000000	.000034	.000000
.7	.33126 (-3)	-2.8983	1.000000	.000097	.0023 (-6)
.8	.81754 (-3)	-2.8655	1.000000	.000241	.0145 (-6)
•9	1.7987 (-3)	-2.8273	1,000000	.000534	.0713 (-6)
1.0	3.6101 (-3)	-2.7834	•9 <b>9</b> 9999	.001082	.2928 (-6)
1.1	6.71% (-3)	-2.7333	. 999998	.002037	1.0374 (-6)
1.2	.0117394	-2.6768	• 9999 <del>9</del> 4	.003605	3.2489 (-6)
1.3	.019426	-2.6136	.999982	.006049	9.1484 (-6)
1.4	.030663	-2.5437	· 999 <b>95</b> 3	.009701	.023529(-3)
1.5	.046427	-2.4669	.999888	.014949	.055872(-3)
1.6	. •067735	-2.3838	•999753	.022236	.123623(-3)
1.7	.095583	-2.2949	· 999 <sup>4</sup> 86	.032045	.25679 (-3)
1.8	.13087	-2.2009	. 99899	·Ontie88	.50394 (-3)
1.9	.17435	-2.1028	.99812	.061267	.93930 (-3)
2.0	.22655	-2.0018	• <b>99</b> 666	.081679	1.6706 (-3)
2.1	.28776	-1.8990	. 99431	.106562	2.8470 (-3)
2.2	.35801	-1.7957	. 99067	.136256	4.6652 (-3)
2.3	.43708	-1.6932	.98525	.17112	7.3747 (-3)
2.4	.52455	-1.5925	· 977 <sup>44</sup>	.21120	.0112790
2.5	.62305	-1.4914	• 96653	.25654	.016734
2.6	.72209	-1.4004	.95172	.30697	.024140
2.7	. 83063	-1.3102	.93213	.36212	.033934
2.8	·94456	-1.2248	.90685	.42145	.046575
2.9	1.06307	<b>-1.1</b> <sup>4</sup> 39	. 87496	·#8#50	.062521
3.0	1.18537	-1.0683	.83557	.54939	.085516

### 1.4

<u>x</u>	_8	Δ	cos26	sin28	sin <sup>2</sup> 6
.1	.090573 (-12)	-3.9986	1.000000	.000000	000000
.2	.046175 (-9)	<del>-</del> 3.99 <sup>4</sup> 3	1.000000	.000000	.000000
.3	1.7625 (-9)	-3.9871	1.000000	.000000	.000000
.4	.023239 (-6)	-3.9770	1.000000	.000000	.000000
.5	.17092 (-6)	<b>-3.</b> 96 <sup>4</sup> 0	1.000000	.000000	.000000
•6	.86802 (-6)	-3.9480	1.000000	.000000	.000000
.7	3.4110 (-6)	-3.9290	1.000000	.000000	.000000
.g	.0111006 (-3)	-3.9068	1.000000	.000002	.000000
•9	.031256 (-3)	-3.8813	1.000000	.000007	.000000
1.0	.078456 (-3)	-3.8526	1.000000	.000018	.000000
1.1	.17934 (-3)	-3.8203	1.000000	.000041	.000000
1.2	.37920 (-3)	-3.7843	1.000000	.000055	.0019 (-6)
1.3	<b>.</b> 75 <b>0</b> 56 (-3)	-3.7445	1.000000	.000175	.0076 (-6)
1.4	1.40354 (-3)	<b>-3.7005</b>	1.000000	.000329	.0271 (-6)
1.5	2.4977 (-3)	-3.6521	1.000000	.000592	.0875 (-6)
1.6	4.2544 (-3)	<b>-</b> 3 <b>.5990</b>	1.000000	.001018	-2589 (-6)
1.7	6-9694 (-3)	-3.5410	•999999	.001685	.7097 (-6)
1.8	.0110227	-3.4777	•9999%	.002696	1.8175 (-6)
1.9	.016555	-3.4090	•999991	.004184	4.3757 (-6)
2.0	.025121	-3.3345	•999980	.006312	9.95% (-6)
2.1	.036381	<b>-3.</b> 2542	•999957	.009250	.021532 (-3)
2.2	.051389	-3.1681	.999911	.013326	.044397 (-3)
2.3	.070917	-3.0763	.999825	.018719	.087608 (-3)
2.4	.095760	-2.97 <b>9</b> 0	•999668	.025763	.165% (-3)
2.5	.127492	-2.8763	-999395	.034787	.30263 (-3)
2.6	·16444	-2.7702	. 99893	.046140	.53251 (-3)
2.7	.20961	-2.6600	.99820	.060008	.90105 (-3)
2.8	.26270	-2.5469	.99702	.077253	1.49424 (-3)
2.9	. 32405	-2.4320	.99522	.097702	2.3921 (-3)
3.0	•39377	-2.3163	•99255	.121829	3.7244 (-3)

## *l* = 5

<u>x</u>	_8	Δ	co=26	sin26	sin <sup>2</sup> 6
.1	.0111855 (-15)	-4.9989	1.000000	.000000	.000000
.2	.022832 (-12)	-4.9955	1.000000	.000000	.000000
•3	1.9639 (-12)	-4.9900	1.000000	.000000	.000000
•#	.046139 (-9)	-4.9822	1.000000	.000000	.000000
•5	.53176 (-9)	-4.9721	1.000000	.000000	.000000
•6	3 <b>.</b> 9028 (-9)	-4.9597	1.000000	.000000	.000000
-7	.020964 (-6)	-4.9451	1.000000	.000000	.000000
.8	.089554 (-6)	-4.9282	1,000000	.000000	.000000
.9	.32097 (-6)	<del>-1</del> 1.9088	1.000000	.000000	.000000
1.0	1.00112 (-6)	-4.8870	1.000000	.000000	.000000
1.1	2.1892 (-6)	-4.8652	1.000000	.000000	.000000
1.2	7.0764 (-6)	-4.8361	1.000000	.000000	.000000
1.3	.016588 (-3)	-4.8067	1.000000	.000003	.000000
1.4	.036341 (-3)	<del>-4</del> .7747	1.000000	.000007	.000000
1.5	.075071 (-3)	-4.7399	1.000000	.000014	.000000
1.6	.147293 (-3)	-4.7022	1.000000	.000028	.000000
1.7	.27611 (-3)	-4.6617	1.000000	.000053	.000000
1.8	.49691 (-3)	-4.6178	1.000000	.000096	.0023 (-6)
1.9	.86205 (-3)	-4.5707	1.000000	.000168	.0070 (-6)
2.0	1.44658 (-3)	-4.5201	1.000000	.000283	.0201 (-6)
2.1	2.3548 (-3)	-4.4657	1.000000	.000465	.0542 (-6)
2.2	3.7278 (-3)	-4.4075	1.000000	.000744	.1383 (-6)
2.3	5.7511 (-3)	-4.3450	•999999	.001159	·3357 (-6)
2.4	8.6625 (-3)	-4.2782	999998	.001764	.7779 (-6)
2.5	.0128411	-4.2067	•999997	.002628	1.7268 (-6)
5.6	.018403	-4.1304	•999993	.003837	3.6816 (-6)
2.7	.026023	-4.0490	. 999985	.005498	7.5581 (-6)
2.8	.036117	-3.9624	.999970	.007739	.0149748 (-3)
2.9	.0,135,116	-3.8706	·99 <b>99</b> 43	.010713	.028690 (-3)
3.0	.066015	-3.7734	·99 <del>9894</del>	.014594	.053250 (-3)

## *l* = 6

Ä		Δ	gos 28	1n 26	ein &
_					
.1	.92461 (-21)	-5.9991	1.000000	.000000	.000000
.2	7.3902 (-18)	<del>-5</del> .9964	1.000000	•000000	•000000
.3	1.46343 (-15)	-5.9918	1.000000	•000000	•000000
•#	.061208 (-12)	-5.9854	1.000000	.000000	•000000
•5	1.10428 (-12)	<b>-</b> 5.9772	1.000000	.000000	•000000
•6	.0116971 (-9)	<b>-5.</b> 9671	1.000000	•000000	•000000
•7	.085749 (-9)	-5.9552	1.000000	•000000	•000000
.8	.47992 (-9)	-5.9414	1.000000	.000000	•000000
.9	2.1 <b>5</b> 47 (-9)	-5.9258	1.000000	.000000	•000000
1.0	<b>8.44</b> 63 (-9)	-5.9081	1.000000	•000000	.000000
1.1	.025601 (-6)	-5.8886	1.000000	.000000	•000000
1.2	.086782 (-6)	-5.8671	1.000000	.000000	•000000
1.3	.24005 (-6)	-5.8436	1.000000	•000000	•000000
1.4	.61353 (-6)	-5.8181	1.000000	•000000	•000000
1.5	1.46437 (-6)	-5.7905	1.000000	.000000	.000000
1.6	<b>3.2921</b> (-6)	-5.7608	1.000000	.000001	•000000
1.7	7.0198 (-6)	-5.7289	1.000000	.000001	.000000
1.5	.0142806 (-3)	-5.6949	1.000000	.000002	.000000
1.9	.027851 (-3)	-5.6584	1.000000	.000005	.000000
2.0	.0522e4 (-3)	-5.6198	1.000000	.000008	.000000
2.1	.094811 (-3)	-5.5787	1.000000	.000015	.000000
2.2	.16657 (-3)	-5.5349	1.000000	.000027	•000000
2.3	.28428 (-3)	-5.4886	1.000000	.000047	.000000
2.4	.47231 (-3)	-5.43%	1.000000	.000078	.0015 (-6)
2.5	.77039 (-3)	-5.3877	1.000000	.000128	.00 <sup>11</sup> (-6)
2.6	1.21222 (-3)	-5.3327	1.000000	.000204	.0104 (-6)
2.7	1.7273 (-3)	-5.2746	1.000000	.000319	.0255 (-6)
2.8	2.8530 (-3)	-5.2131	1.000000	.000489	.0597 (-6)
2.9	4.2508 (-3)	-5.1480	1.000000	.000735	.1350 (-6)
3.0	6.2197 (-3)	-5.0792	• 999999	.001086	.2947 (-6)

# *L* = 7

X.	_8_	Δ	<u>cos 2</u> δ	sin 28	ein <sup>2</sup> 6
.1	.054718 (-24)	-6.9992	1.000000	.000000	.0000000
.2	1.7889 (-21)	<b>-</b> 6•9969	1.000000	.000000	.000000
•3	.75032 (-15)	<del>-</del> 6.99 <b>30</b>	1.000000	.000000	.000000
.4	.058079 (-15)	-6.9877	1.000000	.000000	.000000
•5	1.6393 (-15)	-6.9807	1.000000	.000000	.000000
•6	.025043 (-12)	-6.9723	1.000000	.000000	.000000
•7	.25034 (-12)	-6.9622	1.000000	.000000	.000000
.8	1.8339 (-12)	<del>-</del> 6.9506	1.000000	.000000	.000000
.9	.0105917(-9)	-6-9374	1.000000	.000000	.000000
1.0	.050692 (-9)	<b>-</b> 6.92 <b>25</b>	1.000000	.000000	.000000
1.1	.20833 (-9)	-6.9061	1.000000	.000000	.000000
1.2	.75480 (-9)	-6.8881	1.000000	.000000	.0000000
1.3	2.4593 (-9)	-6.86 <b>8</b> 4	1.000000	.000000	.000000
1.4	7.3189 (-9)	<b>-6.8471</b>	1.000000	.000000	.000000
1.5	.020140 (-6)	-6.8545	1.000000	.000000	.000000
1.6	.051755 (-6)	-6.79 <del>9</del> 4	1.000000	.000000	.000000
1.7	.125211 (-6)	<b>-</b> 6.772 <b>9</b>	1.000000	.000000	.000000
1.5	.28710 (-6)	-6.7447	1.000000	.000000	.000000
1.9	.62745 (-6)	-6.7148	1.000000	.000000	.000000
5.0	1.31318 (-6)	-6.6830	1.000000	.000000	.000000
2.1	2.64 <b>2</b> 6 (-6)	-6.6495	1.000000	.000000	.000000
2.2	<b>5.</b> 1311 (-6)	-6.6139	1.000000	.000001	.000000
2.3	9.6420 (-6)	-6.5764	1.000000	.000001	.000000
, 2 <b>.</b> 4	.017581 (-3)	-6.5370	1.000000	.000002	.000000
2.5	.031377 (-3)	-6.4955	1.000000	.000004	.000000
5.6	.053878 (-3)	-6.4519	1.000000	.000008	.000000
2.7	.083575 (-3)	-6.4061	1.000000	.000013	.000000
2.8	.149956 (-3)	-6.3581	1.000000	.000022	.000000
2.9	.24225 (-3)	-6.3077	1.000000	.000035	.000000
3.0	.38365 (-3)	-6.2549	1.000000	.000056	.000000